
A Reconstruction Method of Large Shaped Reflective Surface Antenna Based on Zernike Polynomials and Least Squares Method

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The shaped reflector antenna enhances the effective radiation of the target area by optimizing the shape of the reflector surface so as to meet the requirements for the complicated working environment and diversified operating modes. And it's significant precondition and foundation of the compensation and the precise switching of the surface shape for the large active reflector antenna active surface to ensure the accurate reconstruction. In view of the long reconstruction cycle disadvantages of the traditional optimization algorithms (such as genetic algorithm), Zernike polynomials based on orthogonal basis functions combined with least squares method is used in this paper to get trigonometric coefficients of the reconstruction equations. Besides, comparing with the optimization algorithm we have proved the correctness and accuracy of the algorithm. Numerical results show reflective surface accuracy of 0.042968 mm by using this method to reconstruct the main reflect surface of the 110-meter aperture antenna to provide the necessary global antenna reflector precision information for switching and performance compensation in different frequency bands.

Shaped reflector antenna surface reconstruction equations can be expressed by Zernike polynomials as:

$$z(\rho, \theta) = \sum_{n=0}^N \sum_{m=0}^M [C_{mn} \cos(m\theta) + D_{mn} \sin(m\theta)] R_n^m(\rho) \quad (5)$$

The exact form of Zernike polynomials of the reflector surface is determined by the projection azimuth and radial index schemes (N, M). Written coefficients equations as a matrix form $A * X = \beta$:

Where,

$$A = \begin{bmatrix} Q & \sum_{i=1}^Q (\rho_i \cos \theta_i) & \sum_{i=1}^Q (\rho_i \sin \theta_i) & \sum_{i=1}^Q (2\rho_i^2 - 1) & \cdots & \sum_{i=1}^Q R_M^N(\rho_i) \\ \sum_{i=1}^Q (\rho_i \cos \theta_i) & \sum_{i=1}^Q (\rho_i \cos \theta_i)^2 & \sum_{i=1}^Q (\rho_i \sin \theta_i)(\rho_i \cos \theta_i) & \sum_{i=1}^Q (2\rho_i^2 - 1)(\rho_i \cos \theta_i) & \cdots & \sum_{i=1}^Q R_M^N(\rho_i)(\rho_i \cos \theta_i) \\ \sum_{i=1}^Q (\rho_i \sin \theta_i) & \sum_{i=1}^Q (\rho_i \cos \theta_i)(\rho_i \sin \theta_i) & \sum_{i=1}^Q (\rho_i \sin \theta_i)^2 & \sum_{i=1}^Q (2\rho_i^2 - 1)(\rho_i \sin \theta_i) & \cdots & \sum_{i=1}^Q R_M^N(\rho_i)(\rho_i \sin \theta_i) \\ \sum_{i=1}^Q (2\rho_i^2 - 1) & \sum_{i=1}^Q (\rho_i \cos \theta_i)(2\rho_i^2 - 1) & \sum_{i=1}^Q (\rho_i \sin \theta_i)(2\rho_i^2 - 1) & \sum_{i=1}^Q (2\rho_i^2 - 1)^2 & \cdots & \sum_{i=1}^Q R_M^N(\rho_i)(2\rho_i^2 - 1) \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ \sum_{i=1}^Q R_M^N(\rho_i) & \sum_{i=1}^Q (\rho_i \cos \theta_i)R_M^N(\rho_i) & \sum_{i=1}^Q (\rho_i \sin \theta_i)R_M^N(\rho_i) & \sum_{i=1}^Q (2\rho_i^2 - 1)R_M^N(\rho_i) & \cdots & \sum_{i=1}^Q R_M^N(\rho_i)^2 \end{bmatrix} \quad (10)$$

$$X = [C_{00} \quad C_{11} \quad D_{11} \quad C_{02} \quad \cdots \quad D_{MN}]^T \quad (11)$$

$$B = \left[\sum_{i=1}^Q z_i \quad \sum_{i=1}^Q (\rho_i \cos \theta_i z_i) \quad \sum_{i=1}^Q (\rho_i \sin \theta_i z_i) \quad \sum_{i=1}^Q (2\rho_i^2 - 1)z_i \quad \cdots \quad \sum_{i=1}^Q R_M^N(\rho_i)z_i \right]^T \quad (12)$$

Table 4 Coefficients by LMS and optimization algorithms(N=4,M=4)

Coefficients	LMS	optimization algorithms	Coefficients	LMS	optimization algorithms
C_{00}	10.415743	10.415743	C_{33}	-0.001178	-0.001178
C_{11}	-0.002948	-0.002949	D_{33}	-0.000095	-0.000152
D_{11}	-0.000092	-0.000117	C_{04}	-0.000381	-0.000381
C_{02}	10.415106	10.415107	C_{24}	0.000473	0.000473
C_{22}	0.002452	0.002453	D_{24}	-0.000030	0.000518
D_{22}	0.000197	0.000311	C_{44}	0.000318	0.000318
C_{13}	-0.001510	-0.001511	D_{44}	0.000043	0.000071
D_{13}	-0.000020	-0.000235	Accuracy	0.042968mm	0.044671mm

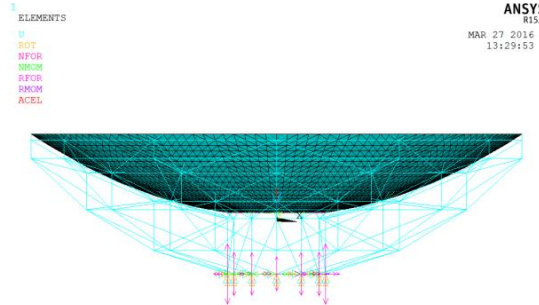


Fig.2 110-meter aperture antenna ANSYS model

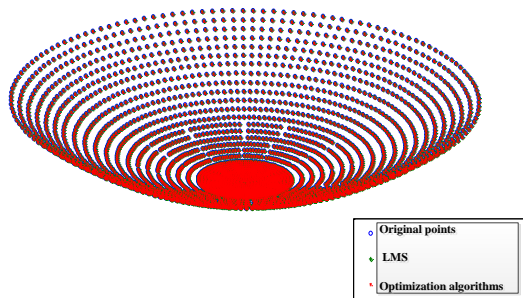


Fig.2 Discrete points expressed by LMS& optimization

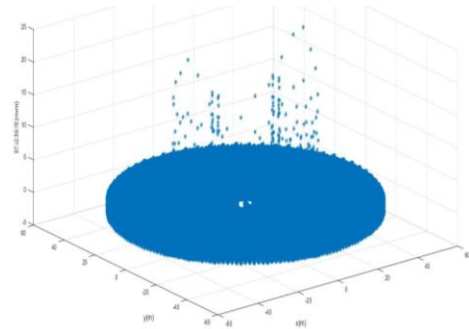


Fig.3 Error distributions between LMS& optimization



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