

APPENDIX F. PROGRAM LISTINGS.

The listings below were obtained during compilation on a PDP11/10 minicomputer. FORTRAN line numbers added during the compilation are shown at the left of each FORTRAN statement. These numbers can be used in reporting any problems to the author. Columns 73 to 80 of many lines have been used for a short comment indicating the purpose of the line, and these are not part of the program code.

The compilations shown were obtained under FORTRAN 4. The programs have been run without modification on some systems using FORTRAN 77. With other machines a few changes may be required. The 'constants' given in DATA statements must retain their values between successive calls to the subroutines. This is not mandatory in FORTRAN, and with some versions of FORTRAN 77 the DATA must be changed to SAVE or STATIC. For systems which carry out run-time checking of array bounds, most of the DIMENSION statements must be changed from FV(40), HT(40) to FV(8), HT(8). Some compilers may also require that statements of the type: DO ## I=1, N+5 be replaced by: N5= N+5 / DO ## I=1,N5.

In the listings below, program statements which are a necessary part of the calculation are shown in upper case. Lines in lower case relate to output listings or trace facilities, and can be ignored for purposes of following the basic program logic.

F.1 THE MAIN SUBROUTINE POLAN

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-----
0001      SUBROUTINE POLAN (N,FV,HT, FB,DIP,START, AMODE,VALLEY,LIST)
c
c - - Generalised POLynomial real height ANalysis - -      may73/feb84.
c Overlapping, Single or Least Squares, with full start and valley options.
c If problems arise, run data with list = 4 and mail all output to:-
c J.E.Titheridge, Physics Dept., University of Auckland, New Zealand.
cXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
c          INPUT DATA
c
c
c--- Polan is called with frequency, height data in the arrays fv, ht.
c
c--- Initially:- set n equal to the dimension of the arrays fv, ht;
c this must be greater than 30 + the number of data points in the arrays.
c
c Intermediate layers terminate at a scaled critical frequency (or fc = 0.)
c with: h' = 0 for a chapman peak and normal valley,
c        h' = 10 for a peak with no following valley,
c        h' = negative for a cusp-type discontinuity only.
c The o-ray fc (scaled or zero) may be followed by an x-ray value (-fcx).
c
c The final layer is terminated by at least 2 null points, with h = f = 0.
c Data can be terminated without a peak by using a final frequency of -1.0.
cXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
c          NORMAL INPUT PARAMETERS
c
c--- FB gives the gyrofrequency at the ground in MHz, for inverse cube.
c
c--- DIP is the magnetic dip angle in degrees.
c
c--- START normally gives a model height at 0.5 mhz. Typical values are:
c noon sunset-2/rise+2hr set/rise set+1hr set+2 set+4 to rise-1
c 85km 88km(E layer) 90(E)/80(F) 100 km 130 km 150 km.
c
c- An extrapolated starting height is used if start = 0.
c- With initial x-ray values a slab start correction is calculated from
c 0.3*fmin (adding points at 0.3, 0.6 and 0.8 *fmin).
c- (With x-ray data, start gives the gyrofrequency height for underlying
c ionisation; the values listed above are still suitable.)
c-----
c--- The final three parameters are zero, for most work.
c
c--AMODE sets the type of analysis, as listed below. Zero uses mode 5.
c Use amode+10 for 12-point integrals, for high accuracy at large
c dip angles (this is done automatically, at dip.ge.60, when amode=0).
c Values of amode greater than 29 are used to specify the number of

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c      polynomial constants to be used to describe each ionospheric layer; *
c      e.g. 80 uses an 8-term real-height polynomial for each separate layer, *
c      85 uses 8 terms for the final layer and 5 terms for lower layers. *
c
c--VALLEY= 0.0 or 1.0 to use the initial default width of twice the local *
c      scale height. The initial default depth is 0.05 MHz. *
c      The calculated depth is scaled according to (calculated width)**2. *
c--LIST = 0 prints results for the start, peak and valley regions only. *
c      = 1 shows the frequ range and polynomial coefficients at each step.*
c      = 2 adds some start/peak output; 3,4 add more detail for each step.*
cXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
c      RETURNED DATA *
c
c      POLAN returns with frequencies, real heights in the arrays fv, ht. *
c      N = no of data points returned, with peak at fc=fv(n-3), hmax=ht(n-3). *
c      Points at n-2,n-1 and n are extrapolated heights at 0.5, 1.0 and *
c      1.5 scale heights above the peak. *
c      fv(n+1) gives the standard error of the critical frequency, in mhz. *
c      ht(n+1) gives the standard error of the peak height, in km. *
c      fv(n+2) gives the total electron content to the peak in e10/m**2. *
c      ht(n+2) gives the scale height of the peak in km; *
c      (a negative value shows an unreasonable peak extrapn was limited.) *
cXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
c      CHANGES TO NORMAL OPERATION *
c      FB negative to use a constant gyrofrequency fh = -fb. *
c      DIP negative to omit physical checks on the calculated profile segments. *
c      START between 0. and 44. defines the plasma frequency for a model start. *
c      start = -1.0 to use a direct start, from the first scaled point. *
c      start < -1.0 for x-starts to use a polynomial from (-start -1.0) mhz. *
c      AMODE negative to omit physical relations (c3.3) from start/valley calcns.*
c      VALLEY = 10.0 for a monotonic (no valley) analysis. *
c      valley = 5.0 for a maximum-valley (upper reasonable limit) analysis. *
c      valley = 0.1 to 5.0 multiplies the standard valley by this factor. *
c      valley = -.01 to -.99 to use -valley as the initial depth, *
c      (instead of the default value 0.05 mhz). *
c      valley = -1.0 to iterate both valley depth and width for best fit; *
c      (-1.x to iterate from an initial depth of 0.x mhz ). *
c      valley = -2.01 to -30 specifies a fixed valley width of 5*int(-valley) km; *
c      and any decimal part of valley specifies the depth in mhz. *
c      LIST = 5 shows each set of simultaneous equations, in the matrix b(i,j). *
c      6/7/8/9 give more detail for the start/reduction/peak/valley step. *
c      Use list negative to trace only the peak and valley steps. *
c      (-1 gives output for the first starting step also). *
c      List= -10 suppresses all output, even the normal layer summaries.*
cXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
c      STANDARD MODES OF ANALYSIS: *
c      Amode=1.- Linear Lamination analysis (with chapman peaks, and valleys). *
c      Amode=2.- Parabolic Lamination analysis, matching end gradients (= paul). *
c      Amode=3.- Overlapping Cubics, with no spurious oscillations(JATP 1982 p657)*
c      Amode=4.- Fourth Order Overlapping Polynomials (Radio Science 1967 p1169). *
c      Amode=5.- Fifth Order Least Squares fit to 6 points (4 virtual + 2 real). *
c      Amode=6.- Sixth Order Least Squares fit to 8 points (5 virtual + 3 real). *
c      Amode=7.- Sixth Order fitting 7 virtual + 3 real heights; calculate 2. *
c      Amode=8.- Sixth Order fitting 8 virtual + 4 real heights; calculate 2. *
c      Amode=9.- Seventh Order fitting 13 virtual + 6 real heights; calculate 3. *
c      Amode=10. A Single Polynomial, fitting 0.73(nv+2) terms to nv heights. *
c      Amode= 10L, where L is an integer in the range 3 to 15, uses a single *
c      polynomial with L terms to describe each ionospheric layer. *
c      Amode= 10L+M uses L terms for the final layer, and M for earlier layers. *
cXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
c
c      In the program listing, error checking, debug
c      and output statements are in lower case.
c
c      Normal printed outputs from Polan are indicated by ----->
c      Trace outputs and abnormal conditions are shown by **----->
c      Fuller debug outputs obtained with list > 0 ##----->
c
c      Loops are delimited by c.....
c-----

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0002      DIMENSION FV(40), HT(40), IT(20),IV(20),IR(20),IH(20)
0003      COMMON /POL/ B(40,17),Q(18), FH,ADIP, MODE,MOD, FA,HA, TCONT,LBUD

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0004 COMMON /POL/ HS, FC,FCC, SH, PARHT, HVAL,VWIDTH,VDEPTH, XWAT
0005 COMMON /POL/ MAXB,NF, NR,NL, NX, MS,MT,JM, LK, KR,KRM, KV,MF, NC counters
c
c !----- first step -----! !---- following steps -----!
c At MODE = 1 2 3 4 5 6 7 8 9 10 1 2 3 4 5 6 7 8 9 10
0006 DATA IT/1,2, 3, 4, 4, 5, 6, 6, 7,73, 1, 2, 3, 4, 5, 6, 6, 6, 7,73/ nterms
0007 DATA IV/1,2, 3, 4, 5, 7, 8,10,12,35, 1, 1, 2, 3, 4, 5, 7, 8,13,35/ nverts
0008 DATA IR/0,0, 0, 1, 1, 2, 3, 5, 2, 0,-1,-1, 1,-2,-3,-3,-4,-6,-3/ realhts
0009 DATA IH/1,1, 2, 3, 3, 4, 5, 6, 8,28, 1, 1, 1, 1, 1, 1, 2, 2, 3,28/ calchts
c
0010 tcontf(x) = x**j*(fa*(fa/j+2.*x/(j+1))+x*x/(j+2)) polycont
0011 maxb= 40 B rows
c maxb= row dimension of array B. Set IR(10 and 20) to maxb-5
c-----
c$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$ (1) Initialisation $$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
c1 --- (1) Initialisation
c
0012 if(list.gt.1)print10,n,fv(1),ht(1),fb,dip,start,amode,valley,list
0014 10 format ('O#ARGS: N,f1,h1='I4,2F7.2,5X,'fb,dip,start=',3F7.2,
1 5X,'amode,valley,list=',2F7.2, I4 /)
c1 ---
c1.1 Set trace, gyrofreq and mode constants.
0015 ADIP= ABS(DIP)
0016 FH = GIND(FB,-ADIP) groundfh
0017 lbug= list
0018 if (lbug.gt.1) call trace (fv,ht, 0.) ##----->
0020 MODE = ABS(AMODE)
0021 IF (MODE.EQ.0.and.ADIP.GE.60) MODE = 15
0023 IF (MODE.EQ.0) MODE = 5
0025 MOD2 = MODE - MODE/10*10
0026 MOD1 = MOD2
0027 IF (MODE.EQ.10.or.MODE.GE.30) MOD1 = 10 snglpoly
0029 FV(N-1) = -1. end data
c-----
c1.2-- Identify the start method to use, and set the following parameters:-
c fa,ha = the origin (starting point) of the first real-height polynomial;
c lk = 1 / 0 / -1 for o-ray / poly / slab start.
c Move virtual height data to start at fv(31), ht(31). Virtual, real height
c origins are at kr, kv = 1, 31-js (where js=no of freqs added below fmin).
c Add an interpolated point at fv(30),ht(30) to control o-ray starts.
c
0030 CALL SETUP (N, FV, HT, START)
c
0031 DHS = AMINI(HS-HA,0.) for c3.3
c$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
c
c/////////// R E A L H E I G H T A N A L Y S I S L O O P
c
c For each cycle: Calculate one polynomial, with nt terms, from the point **
c fa=fv(k), ha=ht(k) to fit the next nv virtual and nr real hts. **
c (nr negative to include one real height below ha). **
c Calculate a further nh real heights, and set k = k+nh. **
c **
c If a critical frequency is found in k+1 to k+nv+1, calculate up to **
c the preceding freq, and determine a least-squares chapman peak. **
c With x-ray data (-ve freqs) at start or after critical, recalculate ha * * * *
c ****
c Real height origin (fa,ha) is at k=kr; virtual at k=kv. krm=top real. **
c *****
c
c$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$ (2) Prepare Data $$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
c2 --- (2) Prepare Data
c
c2.1 Start of analysis (or restart after a peak)
0032 200 MOD = MOD1 =1 to 10
0033 KRM = KR top real
0034 NNR = 0
0035 GO TO 230
c2.1a Later segments (using mod+10)
0036 210 IF (MOD.GT.10) GO TO 220

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0038          KR = KR-IR(MOD)                                step bak
0039          KV = KV-IR(MOD)
0040          MOD = MOD+10
0041 220      NNR = IR(MOD)                                    real hts
c2.1b
0042 230      NT = IT(MOD)                                     terms
0043          NV = IV(MOD)                                     virtuals
0044          NH = IH(MOD)                                     to calc
0045          NR = IABS(NNR)
0046          NL = MINO(1,NR-NNR)                             prev ht
0047          MS = 0
0048          IF (LK.EQ.1.AND.KV.EQ.29) MS = 1                GradEqua
0050          IF (NV.GT.1.AND.NV.LT.8) NV = NV - MS           at start
-----
c2.2          Count initial x-rays. Check frequency sequencing.
c              Check for cusp, peak, or end of data.
c Set nf= no of o-rays (=nv, if sufficient points exist before a peak/restart);
c   nx= x-rays;   mv= nf+nx;   fm= fv(mf) = top frequency in this step.
c   fcc = fc or 0.1 for a peak, = -.1 for cusp at fm, = 0. otherwise.
c
0052      CALL SELDAT (NV, FV, HT)
c
0053          tras= -2.2
0054          if (nv.lt.0) go to 630                            exit>>>>
0056      FM = FV(MF)                                          top freq
0057      MV = MF-KV                                           # freqs
0058      IF (NF.GT.NV) NH = NH + (NF-NV)/2                    to calc.
0060          if (list.lt.-3.and.list.ge.-9) lbug= 1          summary
0062          if((fcc.gt.0..or.fc.gt.0.)and.list.ge.-9) lbug=iabs(list) trace on
0064          if(lbug.gt.2.or.(lbug.eq.2.and.mod.lt.10))calltrace(fv,ht,2.2) ##----->
0066      IF (KR.EQ.1) GO TO 300                                start
-----
c2.3      Subtract the group retardation due to the last calculated real-height
c section. This modifies all h' at f > fa (where fa = fv(kr)), and increases
c the index lk (giving the height to which group retardation is removed) to kr
c
0068      CALL REDUCE (FV, HT)
c
0069          tras = -2.3
0070          if (jm.le.0) go to 640                            exit>>>>
0072          if (lbug.gt.2) call trace (fv,ht,2.3)           ##----->
-----
c$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$ (3) Set Up Equations for next profile step $$$$$$$$
c3 --- (3) Set Up Equations for next profile step
c
c3.1          Initialise mt,fa,fc and counters.
0074 300      MT = NT
0075          IF (NT.GT.20) MT = (NF+2) *NT/100                mode 10
0077          IF (NX.GT.0) MT = MT + (NX+1) /2                + x-rays
0079          IF (NF.GT.NV) MT = MT + (NF-NV)/3
0081          IF (MODE.LT.30) GO TO 310
0083          MT = MODE/10                                     setterms
0084          IF (FV(MF+2).NE.0..and.MOD2.GE.2.and.NF.LT.NV) MT = MOD2    not last
0086 310      MT = MINO(15,MT,MV+NR+MS)                       terms
0087          JM = MT
0088          FA = FV(KR)                                       newstart
0089          HA = HT(KR)                                       newstart
0090          NC = 0                                           iteratns
c
c              Check for valley, set valley flag hval
c              Initialise valley width and depth
0091      LOOP = 0
0092      CALL STAVAL (FV,HT, START,VALLEY, LOOP)
c
c              Is this a start or valley calcn?
0093      IF (LK.GT.0.and.HVAL.EQ.0.) GO TO 320                not valy
0095          IF (MODE.GE.30) MT= MT-1                        fixedJM
0097          MT = MINO(MT,MV-1)                               polterms
0098          JM = MT+1                                         + offset
0099 320          if (lbug.gt.3) call trace (fv,ht,3.1) ##----->
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c3.2                               Set Up Equations in B
c
0101 330 CALL COEFIC (MV,FV,HT)           setcoefs
0102          tras = -3.2
0103          if (jm.lt.0) go to 640       exit>>>>
0105 IF (AMODE.LT.0..OR.MV+4.GT.MAXB) GO TO 380 no phys
0107 IF (MS.NE.1) GO TO 340
0109          G = 1.0 + 1.8/FV(30)         o start,
0110          B(MV+1, 1) = .5              set Q1
0111          B(MV+1,JM+1)= .5*G*(HT(30)-HA)
0112 340 IF (LK.GE.0) GO TO 360
c3.3                               (add ms physical start relations. x only)
0114          WS = 0.1                     weight
0115          IF (START.GT.44.) WS = 0.5
0117          B(MV+1,JM) = WS
0118          B(MV+1,JM+1) = DHS*1.6 *WS   q(jm)=dh
0119          B(MV+2,MT) = WS*.3
0120          B(MV+2,JM+1) = (HS/3.-20.) *WS*.3 slab
0121          B(MV+3,MT-1) = WS*.3         lowerder
0122          MS = 3
0123          GO TO 380
c
0124 360 IF (HVAL.EQ.0.) GO TO 380
c                               (add ms physical valley relations. x or o)
0126          WV = 1.0                     weight
0127          IF (HVAL.LT.-2.) WV = 10.    fix valy
0129          IF (NX.GT.0) WV = 0.2
0131          B(MV+1,JM) = WV
0132          B(MV+1,JM+1) = (VWIDTH - PARHT) *WV stddvaly
0133          B(MV+2,MT) = 0.5              lowerder
0134          B(MV+3,1) = 0.4               grad-
0135          B(MV+3,JM) = -.1/VDEPTH       -cont.
0136          B(MV+4,MT-1) = 0.15          lowerder
0137          MS = MINO(4, MT)
c
0138 380 NC = NC+1
0139          if(lbug.gt.2.or.(ms.gt.0.and.lbug.ne.0)) call trace(fv,ht,3.3)##----->
c$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$ (4) Real-Height Solution $$$$$$$$$$$$$$$$$$$$$$$$
c4 --- (4) Real-Height Solution
c4.1 Solve equations in B
0141          NS = MINO( MV+NR+MS, maxb)
0142          CALL SOLVE (NS, JM, B, Q, DEVN) calc. q
c
c4.2                               Check physical constraints
c
0143          if (ms .eq. 1) lbug= lbug+200 leave q1
0145          if (dip.lt.0.) lbug= lbug+400 noadjust
0147          Q(18) = DEVN
0148          CALL ADJUST (HA,FA,FM,FC, LK,JM,MT, B,Q, LBUG)
c
c
c4.3                               Iterate a valley or x-start calcn.
0149          LOOP = 2
0150          IF (JM.EQ.MT.or.NX.GT.0) GO TO 420 0-ray Valley; loop once to adjust depth
c
0152          VWIDTH = Q(JM) + PARHT
0153          IF (NC.EQ.1.and.HVAL.NE.0.) LOOP = 1 adj.vdep
0155 420 if(lbug.gt.1.and.hval.ne.0..or.lbug.gt.2)calltrace(fv,ht,4.3)##----->
c
0157          IF (FB.LT.0.) LOOP = -IABS(LOOP) fixed fh
0159          IF (JM.GT.MT) CALL STAVAL (FV,HT, START,VALLEY, LOOP) strt/val
0161          IF (LOOP.EQ.4) GO TO 330       valyloop
0163          IF (LOOP.EQ.3.and.FB.GT.0.) GO TO 330 xrayloop
c$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$ (5) Store Real Heights $$$$$$$$$$$$$$$$$$$$$$$$
c5 --- (5) Store Real Heights
c
0165          KRM= KR+NR-NL                 lastreal
0166          KVM= KV+NR-NL
0167          NH = MINO(NH,NF-MOD1/10*2)     to calc.
0168          MQ = MT+MINO(LK,0)             polterms

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0169      QM = Q(MQ)
0170      KA = KVM + 1                                next pt.
c.....
0171      DO 520 K = KA, MF
0172          FR = FV(K)
0173          KRM = KRM+1
0174          DELTF = FR-FA
0175          FV(KRM) = FR
0176      520    HT(KRM) = HA + SUMVAL(MQ,Q,DELTF,1)
c.....
0177          FN = FV(KVM+NH)
0178          DF = FV(KVM) - FA
0179          IF (FCC.EQ.0.) GO TO 540
0181          NH = KRM-KR                                to peak.
0182          FN = FM
0183      540    DO 560 J = 1, MQ
0184      560    TCONT = TCONT+J*Q(J)*(TCONTF(FN-FA) -TCONTF(DF))        polycont
c
0185          KR = KR+NH                                step on
0186          KV = KV+NH                                origin
0187          FC = FCC
0188          IF (FC.EQ.0.) GO TO 210                    do next
0190          IF (FC.EQ.-.1) GO TO 200                    cusp
c$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$ End of Normal Steps $$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
c$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$ (6) Calculate and List Peak data $$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
c6 ---                                     (6) Calculate and List Peak data
c
c6 ---                                     Least-squares fitting of a Chapman-layer peak.
c
0192          tras= 6.
0193          if (fc.lt.0.) go to 620                      end>>>
0195          if (ht(krm).lt.90.) go to 640                abort>>>
0197      CALL PEAK (FV, HT, HMAX)
c-----
c7 ---                                     (7) Restart for a New Layer, or end.
c7.1
0198      HS = (HMAX + HT(KRM))/2.                        for fh
0199      IF (HT(KV+1).GT.0.) GO TO 200                    newlayer
c
c7.2          All finished. Add points at z = .5, 1.0, 1.5 above peak,
c                                     using a scale height gradient of 0.1.
0201      N = KR + 3
0202      FV(N-2) = FC *.97372
0203      FV(N-1) = FC *.91213
0204      FV(N ) = FC *.83462
0205      HT(N-2) = HMAX + SH *.05128
0206      HT(N-1) = HMAX + SH *.10526
0207      HT(N ) = HMAX + SH *.16216
0208      FV(N+2) = TCONT*.124                              t.e.c.
0209      HT(N+2) = SH                                      scale ht
0210      FV(N+3) = 0.
0211      HT(N+3) = 0.
0212      RETURN
c-----
c7.3          E x i t   o n   E r r o r
0213      620      if (fc.eq.-1.) go to 660
0215      630      if (nv.lt.0) kv = -nv -1                >>seldat
0217      640      if(lbug.ge.-9)print650, (fv(i),ht(i),i=kv-1,kv+3),tras,kv **----->
0219      650      format ('0>>>>>error at f,h ='10f8.3,
                        $ ' section',f4.1,i5,' >>>> end', /)
c
0220      call trace (fv,ht,tras)                          **----->
0221      660      n = kr + 1
0222          fv(n) = fv(kv+1)
0223          ht(n) = ht(kv+1)
0224          fv(n+1) = 0.
0225          ht(n+1) = 0.
0226          return
0227      END

```

## F.2 THE SUBROUTINES SETUP, SELDAT AND STAVAL

Subroutines called by POLAN for preparation of input data for successive steps of the real-height calculation are grouped in a file POLSIN.FOR. The first subroutine SETUP is called only once near the beginning of POLAN to determine basic start constants. These include the smallest values of plasma frequency and virtual height in the data, the start method to be used, and an appropriate extrapolated value for the starting height (used in extrapolated starts, and to define the gyrofrequency in the low-density underlying region). The given data are also moved up to start at positions 31 in the frequency, height arrays, so that calculated real-heights can be filled in from the beginning of the same arrays.

SELDAT is called at the beginning of each new step in POLAN. It determines which data points will be used to calculate the next real-height polynomial, and deletes any unwanted extraordinary ray data.

STAVAL supervises all start and valley calculations within POLAN. It is always called during the initialising phase for each real-height step, to determine whether a valley is involved and to set the valley flag HVAL accordingly. If the following calculation is to determine a valley, initial estimates for the valley width and depth are made, based on a model value for the neutral scale height, and flags are set to control the type and path of the valley iteration.

After a real-height solution involving a start or valley, STAVAL is called again to check the result. Calculations involving extraordinary ray data and a height-varying gyrofrequency are iterated, at least once, adjusting the value of gyrofrequency to match the last-calculated real heights. Valley calculations are also iterated to keep the assumed value of valley depth in a fixed relation to the calculated width. For two-parameter valley calculations an additional iteration loop is required to determine independent values of depth and width to give the smallest r.m.s. error in the fit to the virtual-height data (and to the physically-desirable conditions included in the valley calculation).

```

c POLSIN.FOR = SETUP, SELDAT, STAVAL.
c***** - input processing for Polan.
c
0001      SUBROUTINE  SETUP (N, FV,HT, START)
c ---      (called from section c1.2 of polan) feb84.
c 1. Move the virtual height data up 30 places, to start at fv(31), ht(31).
c 2. Set N = number of data points (up to two zero heights).
c    fmin = the lowest plasma frequency in the data.
c    hmin = the lowest virtual height in the data.
c    (these are used for start extrapolation in the absence of x-ray data).
c 3. Identify the start method, and set the following parameters:
c    js = the number of points added below fmin, = 2/1/0 for oray/xray/direct.
c    fa, ha define the starting point for the first polynomial.
c    hs = the height to evaluate the gyrofrequency for an x-ray start.
c    lk = 1 / 0 / -1 for o-ray / x-ray poly / x-ray slab starts.
c The real and virtual origins are at kr = 1 and kv = 31-js.
c-----
Constants which SETUP sets in /pol/ are:- lk,kr,kv, fa,ha, hs,vdepth.
c
0002      DIMENSION  FV(40), HT(40)
0003      COMMON /POL/ B(40,17),Q(18), FH,ADIP, MODE,MOD, FA,HA, TCONT,LBUG
0004      COMMON /POL/ HS, FC,FCC, SH, PARHT, HVAL,VWIDTH,VDEPTH, XWAT
0005      COMMON /POL/ MAXB,NF, NR,NL, NX, MS,MT,JM, LK, KR,KRM, KV,MF, NC counters
0006      VDEPTH = 0.
0007      VWIDTH = 0.
0008      TCONT = 0.
0009      SH = 0.
0010      FC = 0.

c1.a --      Move virtual data to start at fv(31), ht(31)
c1.a --      Find index j of the 1st o ray; fmin= lowest fn
0011      K = N-30
0012      10      FV(K+30)= FV(K)
0013      HT(K+30)= HT(K)
0014      IF (FV(K).GT.0.) J= K
0016      K = K-1
0017      IF (K.GE.1) GO TO 10
0019      FMIN = FV(J)
0020      IF (J.GT.1) FMIN = AMIN1(FMIN,SQRT(FV(1)*(FV(1)+.9*FH)))

```

```

c1.b --
c1.b --          Set starting conditions (direct, extrap or model).
c              Calculate initial fa, ha;- start from fmin:
0022      HMIN = HT(J)
0023      DO 20 I = 1, 5
0024 20      IF (HT(J+1).GT.45.) HMIN = AMIN1(HMIN, HT(J+1))          h'min
0026      HA = HMIN
0027      FA = FMIN
0028      HS = HA
0029      JS = 0
0030      LK = 1
0031      IF (START.EQ.-1.0.AND.J.EQ.1) GO TO 40                      direct
c              - start extrapn:
0033      JS = 2                                                    add 2pts
0034      DH = ABS(HT(J+2)-HT(J)) *FMIN / (FV(J+2)-FMIN)           to f = 0
0035      HS = AMIN1(HMIN-DH, HMIN/2.+50.)                          start fh
0036      HS = AMAX1(HS, HMIN/4.+55.)                                lowlimit
0037      FA = AMIN1(.5, .6*FMIN)
c              - model height:
0038      IF (ABS(START).GE.45.) HS = AMIN1( ABS(START), HS*.4+HMIN*.6 )  ' model
0040      IF (J.GT.1) GO TO 30                                       x start
0042      HA = HS                                                    start ht
0043      IF (MODE.EQ.10 .OR. MODE.GE.20) FA = FMIN*.6             snglpoly
0045      IF (START.GE.45. .OR. START.EQ.0.) GO TO 40                o start
c              - model density:
0047      H = INT(START*.1)*10
0048      HA = 90.+H+H
0049      FA = START-H
0050      GO TO 40
c              - x-ray calculn:
0051 30      JS = 1                                                    add 1pt.
0052      HA = HS*.4 + HMIN*.6                                       x start
0053      LK = 0
0054      IF (START.GT.-3.) FA = -START-1.                          polystrt
0056      IF (START.LT.-1.) GO TO 40
0058      LK = -1
0059      FA = FMIN*.6                                               slabstrt
0060      VDEPTH = FMIN*.3
c1.c --
c1.c --          Store initial points. Virtual data starts at index kv (29 to 31).
0061 40      KV = 31-JS
0062      FV(30) = (FA + FMIN)/2.0                                     o start,
0063      HT(30) = HMIN - DH*(FMIN-FV(30))/FMIN                      add virt
0064      if (j.eq.1) hs= ht(30)                                     (& show)
0066      FV(KV) = FA
0067      HT(KV) = HA
0068      FV(1) = FA
0069      HT(1) = HA
0070      KR = 1                                                    realstrt
0071      RETURN
0072      END

```

```

c*****
0001      SUBROUTINE SELDAT (NV, FV, HT)
c              called from section c2.2 of polan.    feb84.
c              Select the virtual-height data to be used in the next step of polan.
c              Define the following parameters:-
c              nf = number of o-ray data points to be used
c              (equal to nv, if sufficient good points exist before a peak/restart);
c              nx = number of x-rays points;
c              fm = fv(mf) = highest frequency included in this step;
c              fcc is set equal to zero for a normal (non-peak) step;
c              equal to -.1 for a cusp at fm;
c              equal to a scaled critical frequency (fc), or to 0.1, for a peak.
c-----
0002      DIMENSION FV(40), HT(40)
0003      COMMON /POL/ B(40,17),Q(18), FH,ADIP, MODE,MOD, FA,HA, TCONT,LBUG
0004      COMMON /POL/ HS, FC,FCC, SH, PARHT, HVAL,VWIDTH,VDEPTH, XWAT
0005      COMMON /POL/ MAXB,NF, NR,NL, NX, MS,MT,JM, LK, KR,KRM, KV,MF, NC counters

```



```

c
c  ffit gives the minimum desirable frequency range, for fitting x-ray data.
c  gfit gives the maximum slope dh'/df which should be used in an x-start.
0006  data  ffit,  gfit  / 0.4, 40. /
-----
c2.a          Count initial x rays. Check frequency sequencing.
c2.a          Check for cusp, peak, or end of data.
0007  FCC = 0.                                     no peak
0008  FSX = 0.
0009  FRX = 0.
0010  MF = KV
0011  FS = FV(KV)                                   start f
0012  F1 = 0.
0013  FH = GIND(0., HT(KR))
0014  NF = 0
c.....          Frequency loop (nf = 1 to nv):
0015  10  NF = NF+1
0016  12  MF = MF+1                                 toppoint
0017      FM = FV(MF)                               top freq
0018      FN = FV(MF+1)                             nextfreq
0019      HV = HT(MF)                                top virt
0020      if (lbug.eq.6.and.kr.eq.1)print *,nv,nf, f1,fm  ##----->
0022      IF (FM.GT.FS) GO TO 20
0024      FRX = SQRT(FM*(FM+FH))                    top xray
0025      IF (MF.EQ.KV+1) FSX=FRX                    lst xray
0027      IF (FM.LT.0..AND.FRX.GE.FSX.AND.NF.EQ.1) GO TO 12  x ray.
0029  15  nv = -mf
0030      return
0031  20  IF (F1.EQ.0.) F1 = FM                       error>>>
0033      IF (HV.LT.0..OR.FN.LT.0.) GO TO 40          cusp,end
0035      IF (ABS(HT(MF+1)).LE.30.) GO TO 50          peak
0037      FS = FM
0038      if (fn.le.fm) go to 15                       error>>>
0040      IF (NF+1.LT.NV.AND.MF-KV.LT.MAXB-4) GO TO 10
c.....
c          Check final point
0042      GRAD = (HT(MF+1)-HV) / (FN-FM)
0043      IF (NF+1.EQ.NV.and.(NF.LE.2.or.KR.GT.1.or.GRAD.LT.100.)) GO TO 10 loopfreq
c
c          Leave loop, with nf = no of o rays (.le.nv).
c2.b
c2.b          Check need for additional points.
0045      IF (MOD.GT.10.OR.MOD.LT.4) GO TO 70          end freq
0047      IF (HT(MF+1)-HV.GT.(FN-FM)*GFIT) GO TO 70  retarded
0049      IF (FRX.GT.FSX .AND. FM.GT.FRX) GO TO 70    all x in
0051      IF (FM-F1+.04*(nf-nv).LT.FFIT .OR.FM.LT.FSX) GO TO 10  incr fm
0053      GO TO 70
c          Cusp (fcc =-0.1) or end data
0054  40  FCC = AMIN1(FN, -.1)                        scont.
0055      HT(MF) = ABS(HV)                             (=cusp)
0056      GO TO 70
c          Peak (fcc = 0.1 or scaled fc)
0057  50  FCC = AMAX1(FN,.1)                          f crit.
c
c2.c          Shift data arrays to delete out-of-range x rays (fnr > fm+0.1).
c2.c
0058  70  MX = MF - NF                                lastxray
0059  80  NX = MX - KV                                x rays
0060      IF (NX.EQ.0) GO TO 100
0062      F = FV(MX)
0063      IF (SQRT((F+FH)*F).GT.FM+0.1) GO TO 90      delete
0065      IF (NX.EQ.1) GO TO 100
0067      IF (HT(MX)-HT(MX-1).LT.GFIT*(FV(MX-1)-F)) GO TO 100  grad ok.
0069  90  J = MX
0070  95  FV(J)= FV(J-1)                              move up1
0071      HT(J)= HT(J-1)
0072      J = J-1
0073      IF (J.GE.KV) GO TO 95
0075      KV = KV+1
0076      GO TO 80

```

```

0077 100 IF (NX.EQ.0.AND.KR.EQ.1) LK = 1          no xstrt
0079     RETURN
0080     END

```

```

c*****
0001 SUBROUTINE STAVAL (FV,HT, START,VALLEY, LOOP)          feb84.
c
c   Staval handles all start and valley calculations, in which the
c   real-height polynomial has a constant term [at q(jm), where jm=mt+1]
c   so that the height at the origin [fa,ha] is recalculated.
c-----
c--> The initialising call enters and exits with loop = 0.
c   If this is not a valley calculation (i.e. hval = 0.) then staval just
c   sets the initial weight xwat for any x-ray data, and returns.
c   For a valley calculation (shown by hval.ne.0.)
c   the iteration-flags devl, devll are initialised, and
c   the standard values for valley depth and width are calculated
c   (based on the 'standard scale height' sha).
c
c--> A call with loop = 1 is to adjust the valley depth for a single o-ray
c   iteration. this exits with loop = 4.
c-----
c--> The main call enters with loop = 2.          ( -2 if fb is negative. )
c   Exit with loop = 2 shows that the start/valley calculation is completed
c   and the required real heights have been added to ht.
c   If loop > 2 on exit, polan recycles the valley calculation:-
c   loop = 3 requests a new calculation with a changed gyrofrequency.
c   loop = 4 is to recalculate with a new value of valley depth vdepth.
c-----
0002 DIMENSION FV(40), HT(40)
0003 COMMON /POL/ B(40,17),Q(18), FH,ADIP, MODE,MOD, FA,HA, TCONT,LBUG
0004 COMMON /POL/ HS, FC,FCC, SH, PARHT, HVAL,VWIDTH,VDEPTH, XWAT
0005 COMMON /POL/ MAXB,NF, NR,NL, NX, MS,MT,JM, LK, KR,KRM, KV,MF, NC counters
constants: base, depthfac, depthconst
0006 DATA VBASE, VDEEP, VCONST / 0.6, .008, 20. /
constants: 1st depth, scale, peak-top increase for valley iteration
0007 DATA VAL1, DVAL1, VPEAK / .1001, 6., 1.4 /
constants: xweight, fhht itern limit
0008 DATA WVX, HXERR / 1.0, 2.0 /
c to remember between calls: (next DATA to SAVE for fortran77)
0009 DATA VAL, DVAL, DEVL, DEVL1, HMAX, HDEC, FHHT / 7* 0.0 / to store
0010 sq(x) = sqrt((1.-x)*(1.+x))
c-----
0011 NFB = LOOP          fix fb ?
0012 LOOP = IABS(LOOP)
0013 IF (LOOP.GT.1) GO TO 200
0015 IF (LOOP.EQ.1) LOOP = 4          o ray
0017 IF (LOOP.EQ.4) GO TO 40
c#####
cxl--- First call (with loop = 0) from polan section c3.
0019 tras = -3.1
0020 XWAT = WVX
0021 PARHT = 0.
cxl.a Check for valley, set flag hval
0022 HVAL = HT(KV)          valley
0023 IF (HVAL.EQ. 0.) HVAL = VALLEY
0025 IF (HVAL.EQ. 0.) HVAL = 1.
0027 IF (HVAL.GE.10.) HVAL = 0.          novalley
0029 IF (HVAL.EQ.0.) RETURN          novalley
c-----
c Initialise valley width and depth
0031 HDEC = INT(HVAL) - HVAL
0032 DEVL = 1.E6
0033 DEVL1 = 1.E7
0034 DVAL = DVAL1          valscale
0035 HMAX = HT(KR)
0036 SHA = HMAX*.25-20.          scale ht
0037 HS = HMAX + SHA          vally fh

```

```

0038      SH = SH *VPEAK                                     topside
cx1.b      Set standard width
0039 20  VWIDTH = SHA*2. * ABS(HVAL)                       standard
0040      IF (HVAL.LT.-2.) VWIDTH = INT(-HVAL) *5.         specifid
c-----
c      Set initial depth, or depth adjustment for valley iteration
cx1.c      Standard depth (width calculations iterate here).
c
0042 40  VAL = VWIDTH**2 *VDEEP/(VCONST+VWIDTH)           v. depth
0043      IF (HDEC.GT.0.) VAL = HDEC                       specifid
0045      IF (HVAL.EQ.-1..AND.NX.GT.0) VAL = VAL1         lstdepth
0047      IF (INT(HVAL).EQ.-1.) HVAL = -1.                iterate
c
cx1.d      Peak section (depth calculations iterate here).
0049 60  VDEPTH = VAL*FA/(VAL+FA)                         depth<fa
0050      PARHT = 2.0*SH* SQ(1.-VDEPTH/FA)                par.vall
0051      HA = HMAX + PARHT                                valy bot
0052      IF (NC.EQ.0) FHHT = HA+20.                       field ht
0054      RETURN
c#####
c#####
c      Main call with loop = 2, from polan section c4.3.
c      Start / valley entry, after "solve".
0055 200  tras = -4.3
0056      DEVN = Q(18)
0057      FNL = 0.
0058      DHL = Q(JM)
c
cx2--      Calculate and check real heights
0059 220  IF (NX.LE.0..OR.(DEVN.EQ.0..AND.HVAL.EQ.-1.)) DVAL = -1. list,end
0061      QM = Q(JM)
0062      HR = HA + QM
0063      HN = HR
0064      FN = FA
0065      MC = NC
0066      MV = NF + NX
0067      MQ = MT + MINO(LK,0)
c.....      (real hts stored for coefic recycle)
0068      DO 300 I = 1, MV
0069          HL = HN
0070          FL = FN
0071          FN = FV(KV+I)
0072          IF (FN.LT.0.) FN = SQRT((FN+FH)*FN)
0074          DELTF = FN - FA
0075          HN = HR + SUMVAL(MQ,Q,DELTf,1)
c
0076          if (nc+mc.gt.25.or.start.eq.-.1) go to 300      omittest
0078          if ( (hn-hl)/(fn-fl) .gt. 2.0) go to 300        grad ok.
c
0080          if (nx.gt.0.and.xwat.eq.wvx.and.nc.gt.1) go to 380 redo
0082          a = qm-amax1(5.,abs(qm)/4.)*amax0(1,3-kr)
0083          nqm = int(a*10.01)                               next qm
0084          if (fn.ne.fn1.or.hn-h1.gt.dhl) go to 350       lower qm
0086          if (lbug.ge.-9) print 250, fv(kv+i)          **----->
0088          250      format('Odata/gyrofrequency incompatible at f ='f6.2)
0089          mc = 25                                         noadjust
0090          300      IF (KR+I.LT.KV) HT(KR+I) = HN
c.....
0092          KRM = MINO(KR+MV, KV-1)                       topcalcd
cx3---      Set field ht (and recycle fb).
0093          IF (NC.LE.2) XWAT = WVX
0095          KHx = KR + 1 + NX/3
0096          DHX = HT(KHX) - FHHT
0097          FHHT = HT(KHX)
0098          IF (NC.EQ.1 .OR. ABS(DHX).GT.HXERR) LOOP = 3   reset fb
0100          IF (NX.LE.0.OR.NFB.LT.0.OR.NC.GE.20) LOOP = 2 no reset
0102          IF (KR.GT.1) GO TO 500                         valley
0104          GO TO 400                                       x start
c-----
c      (jump here to get new solution with reduced start offset)

```

```

0105 350          dev = devn
0106          call solve (nqm, -jm, b,q, devn)          decr. qm
0107          if(lbug.gt.0) print360, nc, qm,q(jm), fn,hn, dev,devn **----->
0109 360          format(i3,' staval: qm reduced from'f6.1,' to'f6.1,', to avoid
          $ -ve slope at f,h ='2f7.2,6x,'(devn increases'f6.2,' to'f6.2,')')
0110          fnl = fn
0111          dhl = hn-hl
0112          go to 220
-----
c-----
c          Re-calculate a bad result
0113 380          xwat = wx/2.          bad data
0114          if(lbug.ge.-9)print 390          **----->
0116 390          format (' x ray weights reduced to 1/4.')
0117          loop = 4
0118          return
c*****
cx4---***** X ray Start: slab (.3-.6f1) +poly*****
cx4---
0119 400          SLAB = Q(MT)
0120          IF (LK.EQ.0) SLAB = 0.          polystrt
0122          if(lbug.ge.-9)print 420, nc,qm, slab,devn, jm,nf,nx,ms, fhht ----->
0124 420          format (i3,' start offset ='f6.1,' km, slab'f6.1,
          1          ' km.',6x,'devn',f6.2,' km',i5,' terms fitting',
          2          i3,' 0 +'i2,' X rays +'i2,1h.,6x,'hx ='f6.1)
0125          IF (LOOP.EQ.3) RETURN          reset fb
0127          KD = 1-LK          addedpts
0128          GO TO 700
c*****
cx5---***** Valley: Iterate and print *****
cx5---
0129 500          VWIDTH = QM + PARHT
0130          if (lbug.gt.0.or.dval.lt.0..or.nc.ge.20)
          1          print 520, nc, vwidth,vdepth, devn, jm,nf,nx,ms, fhht ----->
0132 520          format ( i3,' valley',f5.1,' km wide,'f8.2,' MHz deep.'
          1          ,7x,'devn',f6.2,' km', i9,' terms fitting',
          2          i3,' 0 +'i2,' X rays +'i2,10x,'hx ='f6.1)
0133          IF (LOOP.EQ.3) RETURN          reset fb
c
0135          KD = 4
0136          LOOP = 4
0137          VBOT = QM*VBASE
0138          SLAB = QM-VBOT          lin.slab
0139          IF (DVAL.LT.0..OR.NC.GT.25) GO TO 700          end valy
0141          IF (HVAL.EQ.-1.) GO TO 600          iterate
c
c - - - - - Normal cycle: Scale depth as (width)**2 - - - - -
0143          IF (DEVN.GT.DEVL/.9.and.nc.lt.4) GO TO 20          revert
0145          IF (DEVL.LT.1.E6) GO TO 560          end valy
0147          DEVL = DEVN
0148          GO TO 40          loopvaly
0149 560          DVAL = -1.
0150          if (lbug.eq.0) go to 500          listvaly
0152          GO TO 700          end valy
cx6--- - - - - - Vdepth Iteration: choose depth vall or vall*dvall. - - - - -
cx6---
0153 600          IF (DVAL.NE.DVAL1) GO TO 620          iterate
0155          IF (VAL.EQ.VAL1) GO TO 675          1stround
0157          DVAL = 1.+5*COS(.015*DIP)          2ndround
0158          IF (DEVN.LT.DEVL) GO TO 675          continue
0160          VAL = VAL1          revert
0161          GO TO 680
c
0162 620          IF (DEVN.GT.DEVL*.97-.003.AND.DEVLL.LT.1.E6) GO TO 660          end
0164          IF (DEVN.LT.DEVL) GO TO 670          continue
0166          DVAL = 1./DVAL          reverse,
0167          VAL = VAL*DVAL          2ndentry
0168          DEVLL = DEVN
0169          GO TO 680
c - - - - - Interpolate to minimum deviation
0170 660          DMIN = (DEVLL-DEVN)/ABS(DEVLL+DEVN-DEVL-DEVL)*.5 - 1.

```

```

0171          DVAL = -DVAL**AMINI(DMIN, .5)
0172          GO TO 680
c
0173 670      DEVL = DEVL
0174 675      DEVL = DEVL
0175 680      VAL = VAL*ABS(DVAL)
0176          GO TO 60
c-----
cx7---***** Tidy up. Delete x rays. *****
cx7---          Add initial points; kd = 1,2,4 for poly, slab, valy
0177 700      LOOP = 2
0178          if (lbug.eq.6) call trace (fv,ht, tras)
0179          KR = KR + KD
0180          KV = KV + IABS(NX)
0181          IF (KD.EQ.0) RETURN
0182          IF (KD.EQ.1) GO TO 750
c
0186          FBOT = FA - VDEPTH
0187          HT(KR-2) = HA
0188          FV(KR-2) = FBOT
0189          HT(KR-1) = HA+QM*VBASE
0190          FV(KR-1) = FV(KR-2)
0191          IF (KD.LT.4) GO TO 750
0193          HT(KR-3) = HA - 0.5*PARHT
0194          FV(KR-3) = 0.5*SQRT(3.*FA**2 + FBOT**2)
0195          FV(KV) = FA
c
0196 750      HA = HA + QM
0197          IF (KD.LE.2) KR = KD
0199          HT(KR) = HA
0200          FV(KR) = FA
0201          IF (KR.GT.3) GO TO 800
c
0203          HT(1) = HA-SLAB
0204          FV(KV-1) = FA
0205          F1 = FV(KV+1)
0206          IF (LK.EQ.0) FV(KV-1) = (FA+F1)*.5
0208          FV(KV) = (FV(KV-1)+F1)*.5
0209          KV = KV-2-LK
0210          VBOT = 0.
0211 800      IF (KR.GT.1) TCONT=TCONT+FV(KR-1)**2*(VBOT+.5*SLAB)+FA**2*.5*SLAB
1          + PARHT*(FA*FA-VDEPTH*(FA+FV(KR-1)))/3.)
0213          if (lbug.eq.6) call trace (fv,ht,tras)
0215          RETURN
0216          END

```

### F.3 THE PROGRAMS COEFIC, ADJUST and REDUCE

COEFIC and REDUCE are the major subroutines required by POLAN for the work of real-height analysis. Along with the subroutine ADJUST which carries out checks on the result, they make up the file POLSUB.FOR.

The subroutine REDUCE is called first in each real-height cycle. Its purpose is to calculate the group retardation caused by the last section of the real height profile, at all higher frequencies. This retardation is subtracted from the virtual heights which remain to be analysed, so that the stepwise calculation of real-height segments can continue without further allowance for the presence of underlying ionisation. For a frequency range of about 0.5 to 1.0 MHz above the current origin (the starting point for the next real-height section), the virtual heights contain a large component due to group retardation in the last real-height section. Group retardations over this range are therefore calculated by integration of the full polynomial real-height expression for the last step. At higher frequencies the group retardation is smaller and is obtained with sufficient accuracy by a simplified procedure which requires only one value of group index per step but effectively allows for parabolic real-height segments. This simplification is made to speed the analysis. As in most real-height procedures, using reasonably large data sets, most of the time is occupied in calculating values of the group refractive index to use in this reduction step.

The subroutine COEFIC sets up the simultaneous equations which are used to define the polynomial real-height coefficients. These equations occupy successive rows in the array B(40,17). If MV is the number of virtual heights included in this step of the analysis, the first MV rows of B contain the virtual-height coefficients relating the real-height coefficients  $q(1), q(2), \dots, q(JM)$  to the values of  $h''(f) - HA$  at each frequency.  $h''$  is the 'reduced' virtual height, equal to the observed height less the group delay due to ionisation below the height HA, and H is the starting point for the current step in the real-height analysis. Calculation of these virtual-height coefficients uses 5, 12 or 17-point Gaussian integration, as described in section 5 and appendix B.3. Suitable weights are also placed on the coefficients in B, to give a graded weighting to the equations at different frequencies.

COEFIC also places coefficients which define known real heights (in terms of the polynomial coefficients) in the following NR rows of the array B, so that the new solution will include a least-squares fit to NR of the previously determined heights. For valley or start calculations POLAN places MS additional physically-derived conditions into following rows of B, before finding the solution for the complete set of  $MV+NR+MS$  simultaneous equations.

COEFIC is also used by the subroutine REDUCE to perform the accurate reduction of virtual heights, using the full polynomial expression for the previous section of the real height profile to calculate and remove the group retardation due to this section at higher frequencies. This reduction is carried out for MV frequencies above the current real-height origin (FA,HA) when COEFIC is called with the first parameter equal to -MV.

The subroutine ADJUST is called by POLAN immediately after the real-height solution is obtained, to carry out various checks on this solution and see if it is physically acceptable. If not, an additional constraint is added into the set of simultaneous equations and a new least-squares solution obtained. This process is carried out rapidly by the subroutine SOLVE, and gives a new (increased) value for the virtual-height fitting error. For adjustments which involve only the correction of non-physical variations in 'unseen' regions of the profile (at plasma frequencies less than the minimum observed frequency  $f_{min}$ ), the adjustment is revoked if it causes an undesirably large decrease in the accuracy with which the calculated profile fits the virtual height data.

```

c POLSUB.FOR = COEFIC, ADJUST, REDUCE.
c*****
c
0001      SUBROUTINE COEFIC (MV, FV, HT)                                jan77.
c
c Calculate coefficients b(i,j), for the real-height polynomial
c       $h-ha = q(j)*(f-fa)**j$ ;    mt terms, fa=fv(k), ha=ht(k).
c The first mv rows of b give virtual ht coefs at freqs k+1 to k+mv;
c      following nr rows give real height coefs at freqs k+1 to k+nr.
c Adds terms for a linear section at x ray start or above peak.
c Subtracts a parabolic segment (with s.h.=1.40*sh) above peak.
c
c Called with mv -ve (from "reduce", in section 2.3) to reduce the next
c |mv| virtual heights by the delay in the previous section fa to fv(k).

```

```

-----
0002 COMMON /POL/ B(40,17),Q(18), FH,ADIP, MODE,MOD, FA,HA, TCONT,LBUG
0003 COMMON /POL/ HS, FC,FCC, SH, PARHT, HVAL,VWIDTH,VDEPTH, XWAT
0004 COMMON /POL/ MAXB,NF, NR,NL, NX, MS,MT,JM, LK, KR,KRM, KV,MF, NC counters
c
0005 DIMENSION TR(17),W(17), GAUSS(17),FNR(17), FV(9),HT(9)
0006 DATA TR / .046910077,.23076534, .50 ,.76923466,.95308992,
1 .009219683,.047941372,.11504866,.20634102,.31608425,.43738330,
2 .56261670,.68391575,.79365898, .88495134,.95205863,.99078032 /
0007 DATA W / .11846344,.23931434, .28444444,.23931434,.11846344,
a .02358767,.05346966,.08003917, .10158371,.11674627,.12457352,
b .12457352,.11674627,.10158371, .08003917,.05346966,.02358767 /
0008 DATA VB, FTC, GTC / 0.6, 0., 180. /
0009 sq(x) = sqrt((1.-x)*(1.+x))
-----
ccl1 ---
ccl1 --- (1). Set integration order and weights
0010 IRA = 1 use 5 pt
0011 IRB = 5
0012 F1 = FV(KV+1)
0013 IF ((MODE.LT.8.OR.MV.LT.0).AND.F1.GT.0.) GO TO 1
0015 IRA = 6 use 12pt
0016 IRB = 17
0017 1 NFF = IABS(MV) freqs.
c
0018 KM = KV + NFF
0019 FW = FV(KM+1) for wv
0020 IF (FW.LT.1.) FW = FV(KM)*2. - FV(KM-1) at fw=0
0022 I = KV + MINO(NFF, MAXO(MOD-15,2)+NR)
0023 DW = FW - FV(I) for wv=1
0024 DA = FV(KV+NR-NL) - FA for wv=1
0025 KP = KR
0026 IF (PARHT.GT.0.) KP = KR-1 end poly
c
c Set gyrofrequency height
0028 HR = HA + 10.*AMINO(1,KR-1) refln ht
0029 IF (KRM.GT.KR) HR = HT(KR+1) for fh.
0031 IF (KRM.EQ.KR) FTC = FA*1.2
0033 IF (MV.LT.0) GO TO 7
0035 IF (LK.GE.0.OR.KRM.EQ.KR) GO TO 4
c Slab start; set fh level.
0037 DELTF = 0.
0038 GRAD2 = Q(1) - GTC
0039 IF (GRAD2.LT.0.) GO TO 3 normal
0041 2 grad1 = grad2
0042 deltf = deltf + .1*fa
0043 grad2 = sumval(mt-1,q,deltf,2) -gtc
0044 if (grad2.gt.0.and.deltf.lt.fa*.45) go to 2
0046 DELTF = DELTF + .1*FA* AMIN1(GRAD2,0.) / (GRAD1-GRAD2)
0047 3 FTC = (FTC+FA+DELTF)*.5 average
c Clear matrix B
0048 4 DO 5 I = 1, MAXB
0049 DO 5 J = 1, 17
0050 5 B(I,J) = 0.
0051 7 CONTINUE
=====
c##### Loop frequencies: i= 1 to nff normally,
c = 0 to nff to fit 1 back height
0052 I = 1 - NL
0053 IF (I.EQ.0.AND.MOD.NE.12) I = -1 prev ht
0055 IF (MV.LT.0) I = 1
c===== Loop frequencies:
0057 10 IREAL = NFF + NL + MAXO(I,0)
0058 KVI = KV + I
0059 KRI = KR + I
cc2 ---
cc2 --- (2). Frequency and weight
0060 F = FV(KVI)
0061 HV = HT(KVI)
0062 FR2 = F*F

```

```

0063      IF (KRI.LE.KRM) HR = HT(KRI) *.8 +HT(KR+1)*.2      refln ht
0065      FH = GIND(O.,HR)                                      set fh
0066      IF (F1.LT.O.) FH = GIND(O.,HS)                       x calcn.
0068      IF (F.LT.O.) FR2 = F*(F+FH)                          x ray
0070      FR = SQRT(FR2)
c
                                Weighting for least squares analysis
0071      WREAL = 10.
0072      IF (KVI.LT.KV) WREAL = 3.                             back ht.
0074      IF (I.LE.O) GO TO 55                                  realonly
0076      if (fr.le.fv(kr).or.fr.ge.fw.or.parht.gt.2.*sh
$          .or.fr.le.fc.or.nff+nr.gt.40) jm = -jm          fatal>>>
cc      if (jm.le.0)print*,is,nff,i,kvi,kri,f,hv,fw,fr,fc,parht @
                                if (jm.le.0) return          end>>>
0078      IF (MV.LT.O) GO TO 12
0080      WVIRT = 1.
0082      IF(NR.GT.NL.AND.FCC.EQ.O.)WVIRT=SQRT(AMIN1((FR-FA)/DA,(FW-FR)/DW)) taper w
0083      IF (F.LT.O.) WVIRT = XWAT
c-----
c                                Integrate from t = tb (at f=fa) to ta
cc3 ---
cc3 ---                                (3). Set integration range and type
0087 12  TB = SQ(FA/FR)                                       lowerlim
0088      TA = 0.                                             reflectn
0089      IF (MV.LT.O) TA = SQ(FV(KP)/FR)                    upperlim
0091      IF (MV.LT.O) GO TO 20
0093      FTC = AMIN1(FTC,FA*.1+FR*.9)
0094      TC = SQ(FTC/FR)
0095      IF (F1.LT.O.) GO TO 15                             x calcn.
0097      TC = 0.39-.05/COS(.016*ADIP)
0098      IF (TB.LT.1.2*TC.OR.INT(ADIP)-2*IRA.LT.58) GO TO 20 dip60,70
c
c                                Extended (17-point) integration.
0100 15  IRA = 1
0101      IRB = 17
0102      TA = TC                                           sectn 1
0103 20  TD = TB - TA
cc4 ---
cc4 ---                                (4). Retardation in start/peak section
0104      DEPAR = 0.                                         peak sum
0105      DELIN = 0.                                         slab sum
0106      IF (LK.GE.O.AND.PARHT.EQ.O.) GO TO 35
0108      IF (SH.NE.O.) DZ = .5*PARHT/SH                    z at fm
0110      GINDV = 0.
0111      DO 30 IR = 6, 17
0112      IF (LK.LT.O) GO TO 28
0114      TP = SQ(FC/FR*SQ(TR(IR)*DZ))
0115      DEPAR = DEPAR + GIND(F,TP) *W(IR)                  pardelay
0116 28  GINDV = GIND(F,SQ((FA-TR(IR)*VDEPTH)/FR))
0117 30  DELIN = DELIN + GINDV*W(IR)                        lindelay
0118 35  CONTINUE
cc5 ---
cc5 ---                                (5). Group index for polynomial terms
0119      DO 50 IR = IRA, IRB
0120      IF (IR.NE.6.OR.IRA.NE.1) GO TO 45
0122      TD = TA                                           sectn 2
0123      TA = 0.
0124      FH = GIND(O.,HR)                                    refln fh
0125      IF (F.GT.O.) GO TO 45                              not xray
0127      FR2 = F*(F+FH)
0128      FR = SQRT(FR2)                                     refln fr
0129      TD = SQ(FTC/FR)                                     corr. tc
0130 45  T = TR(IR)*TD+TA
0131      FN = SQ(T)*FR
0132      GAUSS(IR) = GIND(F,T)*T*W(IR)/FN *TD*FR2
0133 50  FNR(IR) = FN - FA
c-----
cc6 ---                                (6). Store coefficients in array B
c
0134 55  DO 90 J = 1, JM
0135      RH = (FR-FA)**J                                     real ht.

```



```

0136      DPEAK = 0.
0137      SUM = 0.
0138      IF (KVI.EQ.KV.AND. J.EQ.1) RH = 1.                mode 2
0140      IF (I.LE.0) GO TO 90                               realongly
0142      IF (J.EQ.JM) DPEAK = DEPAR*PARHT                par.peak
0144      IF (J.LT.MT.OR.(J.EQ.MT.AND.LK.GE.0)) GO TO 60
c
c                               Start or valley terms
0146      RH = J-MT
0147      IF (J.EQ.MT) SUM = DELIN                          lin.slabb
0149      IF (LK.GT.0) SUM = aINDV*VB+DELIN*(1.-VB)        lin.valy
0151      GO TO 80
c
c                               Polynomial terms
0152 60      DO 70 IR = IRA,IRB
0153      A = GAUSS(IR)
0154      GAUSS(IR) = A*FNR(IR)
0155 70      SUM = SUM+A
0156      SUM = J*SUM                                       delay
c
c                               Coefficients B(i,j).
0157 80      B(I,J) = (SUM+RH)*WVIRT                       virtual
0158      IF (MV.LT.0) HT(KVI) = HT(KVI)-Q(J)*SIGN(SUM,HV)-SIGN(DPEAK,HV) reduce
0160 90      IF (IREAL.LE.NFF+NR) B(IREAL,J) = RH*WREAL   real
c
0162      IF (MV.LT.0) GO TO 100
c-----
cc7 ---      (7). Store Virt/Real heights as r.h.s.
0164      IF (I.GT.0) B(I,JM+1) = (HV-HA-DPEAK)*WVIRT    V r.h.s.
c
0166      IF (IREAL.GT.NFF+NR) GO TO 100
0168      REAL = HT(KRI) - HA
0169      IF(MOD.EQ.12) REAL = Q(1)+2.*Q(2)*(FA-FV(KR-1)) gradient
0171      B(IREAL,JM+1) = REAL*WREAL                      R r.h.s.
0172 100     I = MAXO(I,0)+1
0173      IF (I.LE.NFF) GO TO 10                          loopfreq
c##### End of frequency cycle =====
0175      RETURN
0176      END
c*****

```

0001 SUBROUTINE ADJUST (HA,FA, FM,FC, LK,JM,MT, BB, Q, LBUG)

```

c                               jan82/jun83.
c Called from section c4.2 of Polan, after the initial call to Solve,
c Adjust is used to condition the real-height polynomial (in df = f-fa)
c   h = ha + df*q(1) + df**2 *q(2) + ... + df**mq *q(mq)
c   by ensuring that
c 1- The gradient dh/df is positive at f = fa.
c   For an 0-ray start calculation, an initial gradient Q1 of
c       greater than 80 km/MHz is reduced to 160.Q1/(80+Q1).
c   For an X-ray slab start (lk =-1) the gradient is limited above 160 km.
c 2- The solution is well-defined:
c   - the last 3 coefficients do not alternate in sign, and
c   - these coefficients have absolute values less than 999.
c   These conditions are omitted for the peak and x-ray start, when a large
c       gradient may be required at one end of the fit range.
c 3- For x start calculations: the underlying slab is positive,
c   the initial height offset is negative,
c   the initial height (+offset) is > 60 km.
c 4- For a valley calculation: the initial gradient dh/df > sha,
c   the initial curvature q(2) < -1.5,
c   the initial height offset is positive.
c
c Adjustments alter the least-squares coefficients q(1) to q(jm),
c   and the rms deviation of the fit devn (stored in q(18)).
c-----
c   When jm = mt, the polynomial ends at mq = mt.
c-----
c   jm = mt+1 and lk.le.0 indicates an x start calculation.
c   The poly then ends at mq = mt-1, and
c   q(mt) = underlying slab thickness, preferably positive;

```

```

c          q(jm) = starting height offset, which must be negative.
c-----
c          jm = mt+1 and lk.gt.0 indicates a valley calculation.
c          The poly then ends at mq = mt,
c          and q(jm) = the valley width, which must be positive.
c-----
c          Adjustments are made by Call Solve (mm, -n, bb, q, devn).
c          This modifies the least-squares solution by adding the constraint
c          q(n) = mm/10., with a weight of 10. Any constraints previously
c          applied at this or larger values of n are first removed by Solve.
c-----
0002      DIMENSION BB(2), Q(18)
c
0003          lflag= (lbug+50)/100                                omit adj
0004          lbug = lbug- lflag*100
c
c          Set mq = no of poly terms, and head
0005      DEVN = Q(18)
0006      MQ = MT
0007      IF (LK.LT.0) MQ = MT-1
0009          if (lbug.eq.-6.and.lk.lt.2) lbug= 96                                start
0011          if (lbug.gt.2.or.(lbug.gt.0.and.lk.lt.2)) print7,(m,m=2,mt) ----->
0013          if (lbug.gt.0.or.(lbug.eq.-1.and.lk.lt.2))
0015      1          print9,'--- ',lk,jm,mt,ha,fa,fm,(q(i),i=1,jm),devn ----->
0016      1          format ('0*adjust---- lk jm mt ha fa fm',6x,
0017      1          'q1',9i9/41x,10i9)
0016      9          format ('*adjust', a6,3i3, f8.2,2f6.2, 10f9.2 /43x,10f9.2)
0017          if (lflag.gt.0.or.jm.lt.4) return                                noadjust
c-----
c(a)          Initial gradient; must exceed 1.5
0019      MINQ1 = 2
0020      IF (LK.GT.1) GO TO 50
c
c          0,X Start: limit gradient to 160,320.
0022          QMAX = 80.
0023          IF (LK.EQ.-1) QMAX = 160.
0025          IF (Q(1).GT.QMAX) MINQ1 = 2.*QMAX*Q(1) / (QMAX+Q(1))
0027          GO TO 60
c
c          Valley: gradient > sha
0028      50      IF (JM.GT.MT) MINQ1 = INT(HA/4.-20.)
c
c
0030      60      IF (Q(1).GE.FLOAT(MINQ1).AND.MINQ1.LT.85) GO TO 80
0032          CALL SOLVE (MINQ1*10, -1, BB, Q, DEVN)                                q(1) adj
0033          if(lbug.gt.0)print9,'q(1)',lk,jm,mt,ha,fa,fm,(q(i),i=1,jm),devn----->
c
c          Valley: initial curvature < -1.5
0035      80      IF (JM.LE.MT.OR.LK.LE.0.OR.Q(2).LT.-1.5) GO TO 100
0037          CALL SOLVE (-15, -2, BB, Q, DEVN)                                q(2) adj
0038          if(lbug.gt.0)print9,'q(2)',lk,jm,mt,ha,fa,fm,(q(i),i=1,jm),devn----->
c-----
c(b)          Check for unnecessary high-order coefficients.
c          Reduce order if last 3 signs alternate, and sizes increasing,
c          or if any size exceeds 999.
0040      100     QQ = Q(MQ)
0041          IF (MQ.LT.5.OR.ABS(QQ).LT.150. .OR.FC.GT.0..OR.LK.LE.0) GO TO 200     o.k.
0043          IF (QQ/Q(MQ-2).GT.2. .AND. QQ/Q(MQ-1).LT.-1.) GO TO 150           fix it
0045          IF (ABS(QQ).LT.999..AND.ABS(Q(MQ-1)).LT.999.) GO TO 200           o.k.
c
c          Add constraint q(mq) = 0., and reduce mq.
0047      150     DEVN = -1.
0048          CALL SOLVE (0, -MQ, BB, Q, DEVN)
0049          if(lbug.gt.0)print9,'mq ',lk,jm,mt,ha,fa,fm,(q(i),i=1,jm),devn ----->
0051          MQ = MQ-1
0052          GO TO 100
0053      200     CONTINUE
c-----
c(c)          S T A R T and V A L L E Y: check sign, and limit offset term
c
0054          DEVL = DEVN
0055          IF (JM.EQ.MT) GO TO 500
0057          IF (LK.GT.0) GO TO 400
c-----
0059          QM = Q(MT)                                Start:- slab

```

```

0060      NQT= 1
0061      IF (QM.GE.0.) GO TO 350
0063 320      CALL SOLVE (NQT, -MT, BB, Q, DEVN)
0064          if(lbug.gt.0)print9,'slab',lk,jm,mt,ha,fa,fm,(q(i),i=1,jm),devn----->
0066      NQT= INT(QM*10.)
0067      IF (DEVN.GT.DEVL*1.25) GO TO 320                      slab= qm
c
0069 350      IOFST = -1                      Start:- offset
0070          IF (Q(JM).GT.0.) GO TO 450
0072          IF (LK.GE.0.OR.HA+Q(JM).GT.60.) GO TO 500
0074          IOFST = 10.*(60.-HA)
0075          GO TO 450
c-----
0076 400      IF (Q(JM).GE.0.) GO TO 500                      Valley
c
0078          IOFST = 1                      Correct initial real-height offset
0079 450      CALL SOLVE (IOFST, -JM, BB, Q, DEVN)
0080          if(lbug.gt.0)print9,'offset',lk,jm,mt,ha,fa,fm,(q(i),i=1,jm),devn----->
c-----
0082 500      Q(18) = DEVN
0083          if (lbug.eq.96) lbug= -6
0085      RETURN
0086      END
c*****

```

0001 SUBROUTINE REDUCE (FV, HT)

```

c
c To reduce the remaining virtual heights by the group retardation in feb84.
c the last calculated real-height section (from fa to fv(kr)).
c
c Modifies all h' at f > fv(kr), by subtracting the group retardation.
c Increases lk (the height to which group retardation is removed) to kr.
c Use LIST = 7 to show details of the reduction steps.
c-----
0002      DIMENSION FV(40), HT(40)
0003      COMMON /POL/ B(40,17),Q(18), FH,ADIP, MODE,MOD, FA,HA, TCONT,LBUG
0004      COMMON /POL/ HS, FC,FCC, SH, PARHT, HVAL,VWIDTH,VDEPTH, XWAT
0005      COMMON /POL/ MAXB,NF, NR,NL, NX, MS,MT,JM, LK, KR,KRM, KV,MF, NC counters
0006      7 format (' reduce:',15f8.3)
c-----
c2.a--      Reduction using full polynomial expression (at f<fm+mode/25).
0007      K = MF
0008      FRED = FV(MF) + .04*FLOAT(MODE)
0009 20      K = K+1
0010      IF (ABS(HT(K)).GT.30..AND.FV(K).LE.FRED) GO TO 20          nextvirt
                                                                reduce k
c---
0012      KV1 = KV+1
0013      KVM = K -1
0014          if(lbug.eq.7)print7, (fv(j),j=kv1,kvm)                minreduc
0016          if(lbug.eq.7)print7, (ht(j),j=kv1,kvm)                maxreduc
0018      CALL COEFIC (KV-KVM, FV, HT)                               ##----->
0019          if(lbug.eq.7)print7, (ht(j),j=kv1,kvm)                ##----->
0021          if (jm.le.0) return                                     prevpoly
                                                                ##----->
                                                                exit>>>>
c-----
0023          do 40 k = kv1, kvm
0024 40          if (abs(ht(k)).lt.ha) go to 50                      Error check on reduced virt hts.
0026          GO TO 60
c
0027 50          list bad point (h'<ha) and delete it
0029 52          if(lbug.ge.-9) print 52, (fv(j),ht(j), j=k-1,k+1) **----->
                                                                format ('0****reduce: data error at f, h =',
                                                                $          6f8.3, i5,' end >>>>')
0030 55          fv(k)= fv(k-1)
0031          ht(k)= ht(k-1)
0032          k= k-1
0033          if (k.gt.kv-4) go to 55
0035          kv = kv1
                                                                move up
c-----
c2.b--      Approx reduction at f>fred for delay in fv(lk) (=fa) to fv(kr)

```

```

0036 60    MQ = MT + MINO(LK,0)                                polterms
0037      LK = MAXO(LK,1)+1
0038      FAR = FV(KR)                                        top freq
0039      G2 = Q(1)
c.....      For section fv(1-1) to fv(1)
0040      DO 100 L = LK,KR                                    loopslab
c                                                    :- Get mean density, thickness
0041      FL = FV(L-1)
0042      FN = FV(L)
0043      AVN = (FL**2+FN*(FL+FN))/3.                          mean f*f
0044      HA = HT(L)
0045      DH = HA - HT(L-1)
c                                                    :- Correct for curvature
0046      DELTF = FN - FA
0047      G1 = G2
0048      IF (FN.NE.FC.AND.FN.GT.FA) G2 = SUMVAL(MQ,Q,DELTF,2)  dh/df.
0050      IF (FN.EQ.FC .OR.FN.LT.FA) AVN = AVN+FN*(FN-FL)/3.  peak
0052      DH = DH+(G2-G1)*(FL+FN)*(FN-FL)**2/(12.*AVN)        correctn
0053      FH = GIND(0.,HA)                                     scale fh
c                                                    :- Loop frequency to end
0054      K = KVM
c---
0055 80      K = K+1                                          loopfreq
0056      F = FV(K)
0057      IF (F.EQ.-1.) GO TO 100                             end freq
0059      FR = F
0060      HV = HT(K)
0061      IF (HV.EQ.0. .AND.HT(K+1).EQ.0.) GO TO 100          end freq
0063      if (abs(hv).le.30.) go to 80                         skippeak
0065      if (f.lt.0.) fr = sqrt((f+fh)*f)
0067      if (fr.lt.far) go to 90                             f error.
0069      TAV = SQRT(1.-AVN/FR**2)
0070      HT(K) = HV - GIND(F,TAV)*DH*SIGN(1.,HV)             reduce
0071      if(lbug.eq.7)print7, f1,fn,tav,dh, f,hv,ht(k)      ##----->
0073      GO TO 80                                           loopfreq
c---      End freq loop. Delete bad data and end
0074 90      if(lbug.ge.-9)print 52, (fv(j),ht(j), j=k-1,k+1), k *****>
0076      fv(k) = -1.                                       end data
c---
0077 100 CONTINUE
c.....
0078      LK = KR
0079      RETURN
0080      END

```

#### F.4. THE SUBROUTINES PEAK, TRACE, SOLVE, SUMVAL AND GIND

This group of five miscellaneous subroutines is contained in the file POLMIS.FOR.

The subroutine **PEAK** is called by POLAN only at the end of the real-height calculations for an ionospheric layer. The gradients at the last several frequencies are used in a least-squares analysis to determine the scale height and critical frequency of the best-fitting Chapman layer. The height of the peak is then found by fitting this layer to the last two calculated real heights. The method used in these calculations is described elsewhere (Titheridge, 1985).

The subroutine **TRACE** is used only to print additional information so that the operation of POLAN can be checked. In normal use, when the input parameter LIST is equal to 0 or 1, this subroutine is never called.

The subroutine **SOLVE (M, N, B, Q, DEVN)** plays an important part in POLAN. Normal operation is obtained when the input parameter N, giving the number of unknowns to be solved for, is positive. Equations specified in the first M rows of the matrix **B** are then solved and results returned as  $q(1)$  to  $q(N)$ . When M is greater than N a least-squares solution is obtained, and the r.m.s. deviation of this solution is returned as DEVN. At  $M = N$  an exact solution is obtained, and  $DEVN = 0$ . In both cases equations of the form

$$b_1q_1 + b_2q_2 + \dots + b_Nq_N = b_{N+1}$$

are stored with the coefficients  $b_1$  to  $b_{N+1}$  in columns 1 to  $N+1$  of the array **B**. Successive equations occupy successive rows in the array; thus the coefficients for the  $i$ th equation are  $B(i,1)$  to  $B(i,N+1)$ . The first M rows of **B** contain coefficients for the M equations to be solved. These are converted to upper triangular form by a series of orthogonal Householder transformations. The rows  $N, N-1, \dots, 1$  are then solved in succession to obtain the parameters  $q_N, q_{N-1}, \dots, q_1$ . This procedure has several advantages over the older method of forming the normal equations and solving them by Gaussian elimination. It is much more stable and gives accurate results for polynomials using 15 or more terms, whereas the normal equations become very ill-conditioned for polynomials of order greater than about 6. The calculations are quite fast, require no row or column interchanges, and can give directly the r.m.s. deviation of the fit. The solution is carried out in place requiring no additional storage. The original equations are destroyed, but the triangulated form retained in the array **B** is directly useful for further examination or adjustment of the results.

**Revised solutions** are obtained by SOLVE when it is called with a negative value for the parameter N. This indicates that an additional equation is to be added into the least-squares solution. The new equation is always  $q_j = M/10$ , where the index  $j$  is equal to  $-N$  and the constant  $M$  is given by the first parameter in the call to SOLVE. Addition of this equation to the previously triangulated set gives  $NP = NQ+1$  equations (where  $NQ$  is the total number of coefficients  $q$ , as given in the first call to SOLVE). These  $NP$  equations are reduced to a new set of  $NQ$  upper triangular results, by application of Givens transformation. The new coefficients  $q$ , and the corresponding value of DEVN, are then obtained.

Before the new solution is obtained in SOLVE the subroutine checks the flags stored in the array ISETQ. These show any constraints previously placed on the coefficients  $q$ . Any previous constraint on the value  $q_j$  is first removed. This is necessary to avoid competition between different constraints, giving a result with an intermediate value of  $q_j$  and a large value for DEVN. Removal of a constraint is achieved by adding in the same equation again, with all coefficients multiplied by  $(-1)^{0.5}$ ; this gives an effective weight of  $-1$  which cancels the effect of the previous constraint. Any existing constraints on  $q_{j+1}$  to  $q_N$  are also removed. Constraints can then be tried successively, at decreasing values of  $j$ , with each trial showing results of only the last constraint. If it is desired to include two separate constraints (on different values of  $q_j$ ) in the final solution, these constraints are applied in order of increasing  $j$ . In all cases the new solution is obtained directly from the previous solution and the stored values of the triangularised matrix  $B_{i,j}$ . Recalculation of group index integrals and of the original coefficients in **B** is not required, so modified solutions are obtained almost instantaneously.

The subprogram **SUMVAL** is used for evaluating various sums and products of arrays, as defined in the listing. This is used by POLAN to obtain the values of real height and gradient from the polynomial real-height coefficients  $q$ , and for some other operations.

The subroutine **GIND** provides values of the group refractive index as a function of the wave frequency  $F$ , and the parameter  $T$  which defines the ratio of plasma frequency to wave frequency. An initialising call with  $T$  negative is used to set the value of gyrofrequency at the ground (GH), and the magnetic dip angle. A height-varying gyrofrequency is normally assumed. Calling GIND with  $F = 0$  scales internal constants to correspond to a height of  $-T$  km. These constants are organised to allow rapid calculation of the values of group index, since this calculation takes most of the time in

a real height analysis. If a fixed value of gyrofrequency is to be used at all heights, the initial value of GH is made negative. The equations used provide results for the ordinary ray when the frequency F is positive, and for the extraordinary ray when F is negative. They are designed to maintain full accuracy for all values of dip angle (from 0 to 90°0), and all values of T (from 0 to 1) for both rays. The derivation of the equations is given in appendix D.3.

```

c POLMIS.FOR = PEAK, TRACE, SOLVE, SUMVAL, GIND.
c***** - utilities for POLAN.
c
0001      SUBROUTINE PEAK (FV,HT, HM)
c*****jan78/dec84.
c Calculate and list parameters for a Chapman-layer peak.
c
c Called with KR, KV pointing at last calculated real height before peak.
c Get FC, SH by a least-squares fit to the last NK calculated heights.
c Include any scaled FC, FCX, and iterate from a model scale height.
c LIST = 8 adds detailed trace outputs.
c-----
0002      DIMENSION FV(9), HT(9)
0003      COMMON /POL/ B(40,17),Q(18), FH,ADIP, MODE,MOD, FA,HA, TCONT,LBUG
0004      COMMON /POL/ HS, FC,FCC, SH, PARHT, HVAL,VWIDTH,VDEPTH, XWAT
0005      COMMON /POL/ MAXB,NF, NR,NL, NX, MS,MT,JM, LK, KR,KRM, KV,MF, NC counters
0006      sq(x) = sqrt((1.-x)*(1.+x))
c-----
c                               Set frequencies
0007      KR = KR + 1                               to peak
0008      KV = KV + 1                               to peak
0009      FM = FV(KRM)                               top ht
0010      HN = HT(KRM) *.999                         ht at fm
0011      NK = MINO(NF*10/(NF+10), KR/3) + 2        f to fit
0012      KA = KV -1 -NK
0013      SH = .27*HN - 21.                           model SH
0014      HM = HN + .3*SH                             for fh
0015      FH = GIND(0., HM)
0016      NKA= NK
0017      IF (FC.GT..1) NK = NK + 1                   incl. fc
0019      FCX = ABS(FV(KV+1))
0020      HCX = HT(KV+1)
0021      IF (ABS(HCX).GT.30..OR.FCX.LT.FM+.5*FH) GO TO 100 no x ray
0023      NK = NK + 1                                 incl fcx
0024      FV(KV+1)= FV(KV)                           swap fc
0025      FV(KV) = FCX                                and fcx
0026      HT(KV+1)= HT(KV)
0027      HT(KV) = HCX
0028      KV = KV + 1
0029 100 grad = .5/fv(ka)
0030      fv(kr) = fc
c-----
c.....                               Set up and solve peak equations
0031      DO 400 J = 1, 2                               iterate
c...
0032      DO 300 I = 1, NK
0033      F = FV(KA+I)
0034      IF (F.EQ.FCX) F = SQRT(FCX*(FCX - FH))        x crit.
0036      W = 2.**((20.*(F-FM)/F))                     weight
0037      T = 0.                                       peak
0038      IF (F.GT.FM) GO TO 260                       f crit.
0040      DELTF = F-FA
0041      GL = GRAD
0042      GRAD = 4./F/ AMAX1( SUMVAL(MT,Q,DELTF,2), 3.) 2dN/dh/N
0043      IF (I.EQ.(NKA+1)/2) GM = GRAD               mean
0045      IF (I.EQ.NKA) GRAD = GRAD *.995             hn corn.
0047      T = SH*GRAD
0048 260 B(I,1) = W                                    *log(FC)
0049      B(I,6) = (ALOG(1.+T)-T)*.25                  save
0050      B(I,2) = B(I,6) *W                            * SH
0051      B(I,3) = ALOG(F) *W                          r.h.s.
0052      if(lbug.eq.8.and.j.eq.2)print *,f,grad,t,b(i,6),w ##----->
0054 300 CONTINUE

```

```

C...
0055          ht(kr) = ht(kv)
0056          fv(kr) = fc
0057          if(lbug.ge.3)print320,nk,nka,sh,(fv(k),ht(k),k=kr-nka-1,kr) ##----->
0059 320      format(' peak fit: nk,nka,sh='2i3,f6.1,2x,14f7.2,(/35x,14f7.2))
C
0060      CALL SOLVE (NK, 2, B, B(1,9), DEVN)
C
0061      IF (GM.GT.1.4*GRAD) GO TO 360                                o.k.
0063          avsh = amax1(b(2,9),0.) *.5 + .5                        use mean
0064          if (b(2,9).gt.1.) avsh = b(2,9)/avsh                    avg 1/SH
0066 340      ms = int(10.*avsh+.5)                                  10* mean
0067          devl = devn
0068          call solve (ms, -2, b, b(1,9), devn)                    imposed
0069          if (devn.gt.devl*2.+01 .or. avsh.eq.1.) go to 360
0071          avsh = 1.                                               sh= sha
0072          go to 340
0073 360      SH = SH*SQRT( ABS(B(2,9)) )
0074          PARHT = SH*AMIN1( ALOG(1.+SH*GRAD), 1.8)                FN to FC
0075          HM = HN + PARHT
0076          FH = GIND(0., HM)
0077          if (parht.gt.sh.or.gm.lt.1.8*grad) go to 500            no itern
0079      CONTINUE
C.....
C----- Form peak parameters
0080 500      FC = EXP(B(1,9))
0081          ERR= 0.5* ( HM-SH*ALOG(1.+SH*GL) -HT(KRM-1) )           fit last
0082          HM = HM - .9*ERR                                         2 hts.
0083          HT(KRM)=HN + .1*ERR
0084          HT(KR)= HM
0085          PARHT = HM - HT(KRM)                                     peaksecn
0086          PARFC = FM/SQ(.5*PARHT/SH) - FM                          FC parab
0087          if(lbug.eq.8)print*,fc,hm,err,parht,parfc
0089          r = 2+nk-nka
0090          fc = amax1( amin1(fc,fm+parfc*r), fm+parfc/r )           limit FC
0091          FV(KR) = FC
C-----
c Check overlap-- this section can be omitted with manual scalings (F monotonic)
0092          FNEXT = FV(KV+1)                                         newlayer
0093          IF (FNEXT.GE.0.) GO TO 620
0095          FNEXT = SQRT(FNEXT*(FNEXT+.99*FH))                       X ray
0096          DO 600 I = 2, 30
0097 600      IF (FV(KV+I).GE.0.) GO TO 610                             1st Oray
0099 610      FNEXT = AMIN1(FNEXT, FV(KV+I))
C
0100 620      IF (FNEXT.LE.0.) FNEXT = FM + 4.*PARFC + .05
0102          FC = AMIN1(FC, FNEXT-.03)
0103          DFC= FV(KR) - FC                                         reduce F
0104          FM = FM - DFC
0105          DEVN= AMIN1(DEVN*2., .5*(FNEXT-FM)/FC)
0106          IF (DFC.LE.0.01) GO TO 680
C
c Layer overlap; reduce frequencies
0108          if(lbug.ge.-9)print640, fv(kr), fc, fnext                **----->
0110 640      format ('0* FC reduced from',f7.3,' to',F7.3,
$           ' since next layer starts at',f7.3,' MHz.' /)
0111          df = dfc/fv(kr)**3
0112          do 660 k = 1, kr
0113 660      fv(k) = fv(k) - df*fv(k)**3
0114          fa = fa - df*fa**3
0115 680      CONTINUE
C-----
c List peak parameters
0116          DEVF = FC*DEVN                                           freq err
0117          BAVGE= -B(2,6) - B(NKA,6)
0118          DEVS = DEVN * SH/BAVGE                                    sh err.
0119          DE VH = DEVN *PARHT/BAVGE + DEVS*SH*GRAD                 hm err.
0120          TCONT= TCONT + PARHT*(FC**2+.5*FM**2) /1.5              parabola
0121          IF (GM.LT.1.4*GRAD) SH = -SH                             -model
0123          if(lbug.ge.-9)print 750, fc,devf, hm,devh,sh,devs, tcont/fc**2 **----->
0125 750      format ('0Peak', F7.3, ' (+/-',F5.3, ') MHz, Height', F6.1,

```

```

1      ' (+/-' ,F4.1,' ) km.   Scale Height',f5.1' (+/-' ,F4.1,
2      ') km.   Slab (to peak) =',F6.1,' km.')
```

0126 FV(KR+4) = DEVF  
0127 HT(KR+4) = DEVH  
0128 FV(KV) = FC  
0129 RETURN  
0130 END

C\*\*\*\*\*

0001 SUBROUTINE TRACE ( FV,HT, TRAS )  
C\*\*\*\*\*jan'79.  
C Full debug listing, produced when 0 < lbug < 10.  
C lbug = 1 produces a single trace line for each real-height step in polan.  
C 2, 3, 4 add fuller trace outputs.  
C lbug > 3 includes intermediate listings of freq,height.  
C lbug = 5 adds a full list of the equations in the matrix B.  
C

0002 DIMENSION FV(40), HT(40)  
C

0003 COMMON /POL/ B(40,17),Q(18), FH,ADIP, MODE,MOD, FA,HA, TCONT,LBUG  
0004 COMMON /POL/ HS, FC,FCC, SH, PARHT, HVAL,VWIDTH,VDEPTH, XWAT  
0005 COMMON /POL/ MAXB,NF, NR,NL, NX, MS,MT,JM, LK, KR,KRM, KV,MF, NC counters  
0006 DATA LIST / 0 / to save

C-----  
0007 IF (IABS(LBUG).GT.9) RETURN no list  
0009 IF (TRAS.NE.0.) GO TO 10  
0011 PRINT 50, 'FRQ', (FV(I), I=1,15) ----->  
0012 PRINT 50, 'HTS', (HT(I), I=1,15)  
0013 LIST = 2 head  
0014 RETURN

C-----  
0015 10 IF (TRAS.EQ.2.2) PRINT 12  
0017 12 FORMAT('0##-----')

C  
0018 IF (TRAS.EQ.2.2 .OR. LIST.GT.1) PRINT 20 ----->  
0020 20 FORMAT ('0##TRACE: kr lk jm mt ha fa frm',  
1 ' krm kv nf nr nl nx ms mode mod hs',  
2 ' fc fcc sh parht hval vwidth vdepth')

C  
0021 FRM = FV(KRM)  
0022 PRINT 25, TRAS, KR,LK, JM,MT, HA,FA,FRM, KRM,KV, NF,NR,NL,NX,MS, ----->  
\$ MODE,MOD, HS, FC,FCC,SH, PARHT,HVAL,VWIDTH,VDEPTH  
0023 25 FORMAT(' ##',F5.1,':',2I4,2I3, F8.2,2F6.2, 9I4, 2X,4F6.2,4F7.2)  
C

0024 LIST = 0  
0025 IF (ABS(TRAS).LT.2.3.OR.LBUG.LT.4.OR.ABS(TRAS-3.3).LT..8) GO TO 60  
C  
C list data, at lbug > 3 and tras =2.3 OR 4.3  
0027 KM = KV+NF+NX  
0028 PRINT 50, 'FRQ', (FV(K), K=KV,KM) ----->  
0029 PRINT 50, 'VHT', (HT(K), K=KV,KM+3)  
0030 PRINT 50, 'RHT', (HT(K), K=KR,KRM)  
0031 50 FORMAT (' #',A3, 16F8.2/ 5X,16F8.2)  
0032 LIST = 1  
0033 60 IF (ABS(TRAS).NE.3.3 .OR. LBUG.NE.5) RETURN

C-----  
C list matrix B, at lbug = 5 and tras = 3.3 only.  
0035 NCOL = IABS(JM)+1  
0036 PRINT 70, (J, J = 1, NCOL) ----->  
0037 70 FORMAT (' ### equations J =', I4, 12I9)  
C...  
0038 NLINE = NR+NF+NX+MS  
0039 DO 80 LINE = 1, NLINE  
0040 80 PRINT 90, LINE, (B(LINE,ICOL), ICOL=1,NCOL) ----->  
0041 90 format (' # matrix b, line', I3, 12F9.4)  
C...  
0042 LIST = 2  
0043 RETURN  
0044 END

C\*\*\*\*\*



```

0001          SUBROUTINE SOLVE (M, N, B, Q, DEVN)
c*****jan77.
c Solve m simultaneous eqns in n unknowns, given in the array B(m,n+1).
c The result is returned in Q(1) to Q(n).
c-----
c   Adjustments to a previously obtained solution may be made by
c   call solve (mm, -n, B, Q, devn).
c This modifies the least-squares solution by adding the constraint
c   Q(n) = mm/10., with a weight of 10.
c Any number of the coefficients Q can be modified in this way.
c
c   When a constraint is applied to Q(n), any constraints
c previously applied at larger values of n are first removed by solve.
c Previous constraints at smaller values of n remain.
c Addition of constraints is numerically stable;
c the removal of constraints is less accurate but still o.k.
c-----
0002          DIMENSION B(40,17), Q(18), ISETQ(17)
0003          DATA NQ, NP, ISETQ / 19*0 /
c              (Change above DATA to SAVE for fortran 77).
0004          IF (N.LT.0) GO TO 3
0006          NQ = N
0007          NP = N+1
c
c              Householder transformations
0008          K = 0
0009 1         K = K+1
0010          ISETQ(K) = 999
0011          S = 0.
0012          MK = M-K+1
0013          IF (MK.LE.0) GO TO 7
0015          S = SUMVAL(MK,B(K,K),B(K,K),3)
0016          IF (K.EQ.NP) GO TO 7
0018          A = B(K,K)
0019          D = SIGN(SQRT(S),A)
0020          B(K,K) = A+D
0021          C = A*D+S
0022          DO 2 J = K+1, NP
0023             S = SUMVAL(MK,B(K,K),B(K,J),3)/C
0024             DO 2 I = K, M
0025 2         B(I,J) = B(I,J)-B(I,K)*S
0026          B(K,K) = -D
0027          GO TO 1
c-----
c              remove any previous constraints on q(n) to q(nq);
0028 3         NN = IABS(N)-1
0029          REMOV = -1.
0030 4         NN = NN+1
0031          IF (ISETQ(NN).NE.999) GO TO 5
0033 51        IF (NN.LT.NQ.AND.DEVN.NE.-1.) GO TO 4
c              add constraint Q(n)=m*.1 (Givens transformation).
0035          NN = IABS(N)
0036          REMOV = 1.
0037          ISETQ(NN) = M
0038 5         Q(NP) = ISETQ(NN)
0039          IF (REMOV.LT.0.) ISETQ(NN) = 999
0041          Q(NN) = 10.
0042          DO 6 I = NN, NP
0043             BII = B(I,I)
0044             R = SQRT( AMAX1(BII**2+Q(I)**2*REMOV, .1E-9) )
0045             C = BII/R
0046             S = Q(I)/R
0047             DO 6 J = I, NP
0048                QJ = Q(J)
0049                IF (I.EQ.NN.AND.J.NE.I.AND.J.NE.NP) QJ = 0.
0051                Q(J) = C*QJ-S*B(I,J)
0052 6         B(I,J) = C*B(I,J)+S*QJ*REMOV
0053          IF (REMOV) 51,51,8
c-----
c              back substitution
0054 7         B(NP,1) = M

```

```

0055      B(NP,NP)= SQRT(S)
0056 8     DEVN = ABS(B(NP,NP))/SQRT(B(NP,1))
0057      DO 10 II = 2, NP
0058          I = NP-II+1
0059          S = B(I,NP)
0060          DO 9 J = I+1, NQ
0061 9         IF (II.GT.2) S = S - Q(J)*B(I,J)
0063 10      Q(I) = S/B(I,I)
0064      RETURN
0065      END

```

```

0001      FUNCTION SUMVAL (N, A, B, L)
c*****jan77.
c Returns the sum for j = 1 to N of:-
c   a(j)*b**j at L = 1 ;   j*a(j)*b**(j-1) at L = 2 (using b = B(1)).
c   a(j)*b(j) at L = 3 ;   a(j)*b(1-L+j*L) at L > 3 (giving LL = 4).
c-----
0002      DIMENSION A(9), B(9)
0003      J = N
0004      S = 0.
0005      LL= MINO(L,4)
c.....
0006 9     GO TO (1,2,3,4), LL      loop from j = n to j = 1.
c
c   L = 1; evaluate polynomial a(j)*b**j
0007 1     S = (A(J)+S)*B(1)
0008      GO TO 8
c
c   L = 2; calculate gradient sum a(j)*j*b**(j-1)
0009 2     S = S*B(1)+A(J)*FLOAT(J)
0010      GO TO 8
c
c   L = 3; calculate sum of products a(j)*b(j)
0011 3     JB= J
0012      GO TO 6
c
c   L > 3; sum of a(j)*b(1,j), with L = 1st dim of b
0013 4     JB= (J-1)*L+1
0014 6     S = S+A(J)*B(JB)
c
0015 8     J = J-1
0016      IF (J.GT.0) GO TO 9
c.....
0018      SUMVAL = S
0019      RETURN
0020      END

```

```

0001      FUNCTION GIND (F, T)
c*****jan77.
c Group index subroutine, for o or x rays. (f negative for x ray).
c Gives (group index -1) to full machine accuracy, for any value of t.
c Initialise by call gind(GH,-dip) to set gyrofreq (mhz) and dip (deg).
c GH is ground value; scaled to height h by FH = gind(0.,h), with h>2.
c An initial negative value of GH suppresses the scaling.
c-----
0002      DATA GH,GHNS,GCSCCT, FH,FHNS,FCSCCT,HFH, C,C2 / 9*0. /
c (change data to save for fortran77).
0003      IF (F.EQ.0.) GO TO 2
0005      IF (T.LT.0.) GO TO 1
0007      T2 = AMAX1(T,.1E-9)**2
0008      IF (F) 5,6,6
c
c store ground constants
0009 1     GH = F
0010      FH = ABS(GH)
0011      DIP = -.01745329*T
0012      GHNS = GH*SIN(DIP)
0013      GCSCCT= (GH*COS(DIP))**2*.5/GHNS
0014      GO TO 3
c
c scale constants to height h = t.
0015 2     IF (GH.LT.0. .OR.T.LT.2.) GO TO 4
0017      FH = GH/(1.+T/6371.2)**3
0018 3     FHNS = GHNS*FH/GH

```

```

0019      FCSCCT= GCSCCT*FH/GH
0020      HFH = .5*FHSN
0021      C = FCSCCT+FHSN
0022      C2= C*C
0023 4     GIND = FH
0024      RETURN

c
c          calculate group index gind = mu' - 1.
c          indented sections increase accuracy for x ray.
0025 5     X = (F+FH)*T2
0026      G1 = X-FH
0027      GO TO 7
0028 6     G1 = F*T2
0029 7     G2 = FCSCCT/G1
0030      G3 = SQRT(G2*G2+1.)
0031      IF (F.GE.O.) GO TO 8
0033      G4 = FHSN*(G3-G2)
0034      X = X*(G1-FH)
0035      G5 = -G4*X/ (FHSN*(SQRT(X+C2)+C))
0036      GO TO 9
0037 8     G4 = FHSN/(G2+G3)
0038      G5 = G1+G4
0039 9     G6 = F+G4
0040      G7 = (F*G2*G4/G1-HFH)*(F-G1)/(G3*G6)
0041      GIND = ABS(G7+G6)/SQRT(G5*G6) -1.
0042      RETURN
0043      END

```

### F.5. THE PROGRAM SCION

This mainline program gives an example of a complete real-height analysis procedure using POLAN. SCION controls the scaling of data from a projected ionogram, correction for skewed or non-linear axes; conversion of the digitised values into virtual height and frequency; ordering of separate ordinary and extraordinary ray data in the way required by POLAN; analysis of the data and listing of the calculated real heights. The digitising sections run in conjunction with a Hewlett Packard 9864A digitiser and digitising table, and will need modifying for other equipment. A full description of the operation and use of SCION is given in section 11 of this report.

```

C  -- S C I O N  --      INPUT on UNIT 6,  OUTPUT on UNIT 7.
C
C  Program to perform an N(H) analysis of an ionogram scaled on the X-Y
C  reader, using the generalised polynomial analysis program POLAN.
C  Leo McNamara, August 1978;  ---- John Titheridge, March 1981.
C=====
C-----!
C:- SUMMARY SCALING INSTRUCTIONS.  [...] / [...] denotes alternatives.  !
C:- NULL = bottom left corner,  outside ionogram frame;  !
C:- TL = Top Left corner;  TR = Top Right corner.  !
C-----!
C 1. Scale 0-ray data for first layer.  !
C 2. [scale TL] / [scale FC; scale TR].  !
C  !
C 3. Scale 0-ray data for next layer.  !
C 4. [scale TL] / [scale FC; scale TR].  !
C 5. Repeat steps 3. and 4., until no more 0 data.  !
C  !
C 6. Scale NULL. ( this always denotes 'end of ionogram').  !
C----!
C 7. Scale lowest useable X-ray data (over a range of about 0.6 MHz);  !
C / [or, in the absence of data, scale TL].  !
C 8. [Scale TL] / [Scale FCX for that layer; scale TR].  !
C 9. Repeat steps 7. and 8., for each available layer.  !
C  !
C 10. scale two nulls.  !
C=====

```

```

C-----
C          INPUTS [reads] are marked and numbered by <<<<<1
C
C          Normal PRINTED OUTPUTS are shown by *****1
C
C LOOPS are delimited by C.....
C-----
      DIMENSION HEADC(19), XC(4),YC(4), FM(20),HM(20)
      DIMENSION FMX(20), FMY(20),  HMX(20), HMY(20)
      DIMENSION FOX(100), HOY(100), FXX(50), HXY(50)
      DIMENSION FV(150), HT(150),  FS(120), HS(120)
      EQUIVALENCE (FOX, FV), (HOY, HT), (FXX,FV(101)), (HXY,HT(101))
C-----
900  FORMAT ('1IONOGRAM'I3,//19A4, 'DIP, FB, START =' 5F7.2 )
901  FORMAT (I4,19A4)
902  FORMAT (20F4.0)
904  FORMAT (12F5.0)
907  FORMAT ('0*',6F6.2,4X,6F6.2,4X,6F6.2,4X,2F6.2)
908  FORMAT (12F5.2)
909  FORMAT (/1H0,A5,12F10.3/(6X,12F10.3))
910  FORMAT (1H0,I4,1X, A7,' POINTS DIGITIZED AND DESKEWED'/)
912  FORMAT ( 6( F7.3,F8.2,5X) )
990  FORMAT(/9X'>>>>> DO YOU WISH TO SAVE TAPE7 FOR PLOTTING <<<<<' )
      NDIM = 150
      ION = 0
C//////////
C
C          (A). START OF NEW IONOGRAM:-
C (1). Read comments
C
10   READ (6,901) IEXIT, HEADC          <<<<<1
      IF (IEXIT.EQ.0) PRINT 990
      IF (IEXIT.EQ.0) STOP '*ALL DONE*'
      ION = ION + 1
C-----
C (2). Read dip angle, gyrofrequency, default starting height at 0.5 MHz.
C This default height is used if no suitable X-ray data are provided.
C
      READ (6,904) DIP, FB, START      <<<<<2
      PRINT 900, ION, HEADC, DIP, FB, START *****1
C
C (3). Read in the values of the visible frequency markers, to be scaled.
C count the frequency markers, and list.
C
      READ (6,902) (FM(I),I = 1,20)    <<<<<3
      DO 20 I = 1,20
20   IF (FM(I).EQ.0.0) GO TO 22
22   NFM = I - 1
      PRINT 24 , (FM(I), I = 1, NFM)   *****2
      FORMAT ('OFREQ. MARKERS',20F6.1)
C
C (4). Read in the values of the height markers to be scaled.
C
      READ (6,902) (HM(I), I = 1,20)    <<<<<4
      DO 30 I = 2, 20
30   IF (HM(I).EQ.0.) GO TO 35
35   NHM = I - 1
      PRINT 40, (HM(I), I = 1, NHM)    *****3
      FORMAT ('OHEIGHT MARKRS',20F6.1)
C//////////
C
C          B E G I N   S C A L I N G
C
C          (B). READ THE POSITIONS OF THE FOUR CORNERS OF THE IONOGRAM
C----- (X,Y; clockwise from bottom left).
C
      READ (6,908) (XC(I), YC(I), I = 1,4) <<<<<5
C
C----- Read in the frequency marker positions - max 6 points per line.

```

```

      READ (6,908) (FMX(I),FMY(I), I = 1,NFM), END          <<<<<6
C----- Read in the height marker positions.
      READ (6,908) (HMX(I),HMY(I), I = 1,NHM), END          <<<<<7
C                                     Deskew corners and markers
      XC1 = XC(1)
      YC1 = YC(1)
      CALL DESKEW ( 0, XC, YC)
      CALL DESKEW (NFM, FMX, FMY)
      CALL DESKEW (NHM, HMX, HMY)
C////////////////////////////////////
C
C          (C). READ IN THE O RAY VIRTUAL HEIGHTS AND FREQUENCIES
C
C          Terminate each layer at corner 2 if FC is not scaled,
C          or at corner 3 if FC is scaled.
      N1 = 1
C.....
100      N6 = N1+5
      READ (6,908) (FOX(I),HOY(I), I = N1,N6)          <<<<<8
      N1 = N1+6
      IF (FOX(N6).GT.XC1.OR.HOY(N6).GT.YC1) GO TO 100
C.....
      CALL DESKEW (N6, FOX, HOY)
C
C          Count the number of o-ray points
C          Set zeros at layer terminations.
C.....
      DO 150 I = 1, N6
      F = FOX(I)
      H = HOY(I)
      IF (F.LT.XC(1).AND.H.LT.YC(1)) GO TO 200
      IF (F.LT.XC(2).AND.H.GT.YC(2)) FOX(I) = 0.
      IF (F.GT.XC(3).AND.H.GT.YC(3)) HOY(I-1) = 0.
150 CONTINUE
C.....
C          END of all O-ray data; add another zero.
200 FOX(I) = 0.0
      HOY(I) = 0.0
      I = I + 1
      FOX(I) = 0.0
      HOY(I) = 0.0
      NOP = I
C
C          LIST scaled and deskewed O-ray data          *****4
      PRINT 910, NOP, 'O-RAY'
C
C          PRINT 912, (FOX(I), HOY(I), I = 1, NOP)          *****5
C////////////////////////////////////
C
C          (D). READ IN THE X-RAY VIRTUAL HEIGHT DATA.
C
C          At least one line is necessary here (off-scale point)
      N1 = 1
C.....
300      N6 = N1+5
      READ (6,908) (FXX(I), HXY(I), I = N1,N6)          <<<<<9
      N1 = N1+6
      IF (FXX(N6).GT.XC1.OR.HXY(N6).GT.YC1) GO TO 300
C.....
      CALL DESKEW (N6, FXX, HXY)
C
C          Count the number of X-ray points
C          Set zeros at layer terminations.
C.....
      DO 350 I = 1, N6
      F = FXX(I)
      H = HXY(I)
      IF (F.LT.XC(1).AND.H.LT.YC(1)) GO TO 380
      IF (F.LT.XC(2).AND.H.GT.YC(2)) FXX(I) = 0.
      IF (F.GT.XC(3).AND.H.GT.YC(3)) HXY(I-1) = 0.
350 CONTINUE
C.....

```

```

C                                     END of all X-ray data; add another zero.
380  FXX(I) = 0.0
     HXY(I) = 0.0
     NXP = I
C
C                                     LIST scaled and deskewed X-ray data.
     PRINT 910, NXP, 'X-RAY' *****6
     PRINT 912, (FXX(I), HXY(I), I = 1, NXP) *****7
     PRINT 910
C///////////////////////////////////////////////////////////////////
C
C                                     (E). ALL DATA HAS BEEN READ IN AND DESKEWED.
C                                     Convert the O and X ray positions to frequencies and heights
C                                     using 4-point interpola in marker positions. Preserve zeros.
C
C                                     frequencies (log interpolation)
     CALL INTERP (-NFM, FMX, FM )
     CALL INTERP ( NOP, FOX, FOX)
     CALL INTERP ( NXP, FXX, FXX)
C
C                                     heights
     CALL INTERP (-NHM, HMY, HM )
     CALL INTERP ( NOP, HOY, HOY)
     CALL INTERP ( NXP, HXY, HXY)
C
     PRINT 410
410  FORMAT ('O   CONVERTED TO FREQUENCY AND HEIGHT. '/') *****8
     PRINT 912, (FOX(I),HOY(I), I=1,NOP) *****8
     PRINT 912
     PRINT 912, (FXX(I),HXY(I), I=1,NXP) *****9
C///////////////////////////////////////////////////////////////////
C
C                                     (F). ARRANGE THE SCALED POINTS IN THE ORDER REQUIRED BY POLAN.
C Array positions are NM in combined data, NOV in O-data, NXV in X-data.
     NM = 1
     NOV = 1
     NXV = 1
C-----
C                                     STORE X-ray points, less final null
500  FCX = 0.
     IF (NXV.GE.NXP) GO TO 550
C.....
     DO 520 I = NXV, NXP
         FS(NM) = -FXX(I)
         HS(NM) = HXY(I)
         IF (FXX(I).EQ.0.) GO TO 540
         IF (HXY(I).EQ.0.) GO TO 530
520  NM = NM + 1
C.....
C                                     Save X-ray critical frequency
530  FCX = FXX(I)
540  NXV = I + 2
C
C-----
C                                     STORE O-ray points; retain null at FC
C.....
550  DO 560 I = NOV, NOP
         FS(NM) = FOX(I)
         HS(NM) = HOY(I)
         NM = NM + 1
         IF (FOX(I).EQ.0.) GO TO 580
         IF (HOY(I).EQ.0.) GO TO 570
560  IF (HOY(I).EQ.0.) GO TO 570
C.....
C                                     Delete null after scaled FC
570  I = I + 1
580  NOV = I + 1
     HS(NM-1) = 0.
     IF (FCX-.5*FB.LT.FS(NM-2)) GO TO 590
         FS(NM) = FCX
         HS(NM) = 0.
         NM = NM + 1
590  IF (HOY(NOV).NE.0.0) GO TO 500
C-----
C                                     ---- END DATA ----

```

```

      FS(NM) = 0.0
      HS(NM) = 0.0
C//////////
C
C              (G).  L I S T   A N D   A N A L Y Z E
C
      PRINT 909, 'FREQ ', (FS(I), I = 1, NM)          ****10
      PRINT 909, 'HVIRT', (HS(I), I = 1, NM)         ****10
      PRINT 910
C
C              Write out the data to UNIT7 for plotting purposes
      WRITE (7,980) NM, HEADC
      WRITE (7,981) (FS(I),HS(I),I = 1,NM)
C.....
      DO 940 I = 1, NM
      FV(I) = FS(I)
940      HT(I) = HS(I)
C.....
      N = NDIM
      AMODE = 0.0
C-----
      CALL POLAN (N, FV,HT, FB, DIP, START, AMODE, 0., 0)
C
      PRINT 909, 'FREQ ', (FV(I), I = 1, N)          ****11
      PRINT 909, 'HREAL', (HT(I), I = 1, N)         ****11
C
      WRITE (7,980) N
      WRITE (7,981) (FV(I), HT(I), I = 1, N)
980      FORMAT (14,19A4)
981      FORMAT (6(F6.2,F6.1))
C
C              RETURN FOR NEXT IONOGRAM
      GO TO 10
      END

```

```

      SUBROUTINE DESKEW (N, X, Y)
C
C              To deskew coordinates in an arbitrary quadrilateral frame.
C-----
C(A).          -:* I N I T I A L I Z E *:-
C AT N = 0:-   X(1),Y(1) to X(4),Y(4) give the coordinates of the four
C              corners of the quadrilateral, clockwise from the bottom left.
C-----
C(B).          -:* D E S K E W *:-
C AT N greater than 0:-   Deskew N coordinates in the arrays X, Y.
C=====
      DIMENSION X(9), Y(9), Z(4)
      DATA X1,X2,X3, Y1,Y2,Y3 / 6 * 0.0 /
      NN = N
      IF (N.GT.0) GO TO 60
C-----
C(A).          N = 0 ;   calculate the deskew coefficients
      X1 = X(1)
      Y1 = Y(1)
      X2 = (Y(4)-Y1) / (X(4)-X1)
C
      DO 20 I = 2, 4
20      Z(I) = Y(I) - Y1 - X2 *(X(I) - X1)
      Y2 = (X(2) - X1) / Z(2)
      Z3 = X(3) - X1 - Y2 * Z(2)
      Z4 = X(4) - X1 - Y2 * Z(3)
      X3 = (1. - Z(2)/Z(3)) / Z3
      Y3 = (Z3 - Z4) / (Z(2) * Z3)
C
      NN = 4
C-----
C(B).          N > 0 ;   deskew the arrays X(N), Y(N).

```

```

C.....
60 DO 80 I = 1, NN
    B = Y(I) - Y1 - X2 * (X(I) - X1)
    A = X(I) - X1 - Y2 * B
    Y(I) = B - X3 * A * B
80 X(I) = A - Y3 * A * Y(I)
C.....
    RETURN
    END

```

SUBROUTINE INTERP (M, X, Y)

```

C
C To obtain true values of the variable Y, by interpolating the
C corresponding scaled ordinate X in a previously given marker array.
C **** Uses 4- term polynomial interpolation.
C **** Requires a minimum of 2, but preferably 4, marker points ****
C **** Zeros are not altered.

```

```

C-----
C USE:-
C AT M NEGATIVE, X is an array of N scaled ordinates, corresponding
C to the N reference marker values given in Y(1) to Y(N)
C-----
C AT M POSITIVE, X(1) to X(N) give scaled ordinates,
C Y(1) to Y(N) return the corresponding interp values.
C-----
C The array D(99) stores the marker position (X), its value (Y),
C and corrected differences for each interval.

```

```

    DIMENSION X(20), Y(20), D(99)
C
    DATA D, NM1, NM2, LOG / 99* 0.0, 3* 0 /
C
    N = IABS(M)
    IF (M.GT.0) GO TO 100
    NM1 = N - 1
    NM2 = N - 2
    LOG = 0
    IF (Y(NM1).LT.100. .AND. Y(NM1).GT.0.) LOG = 1

```

```

C=====
C(A). M NEGATIVE:- Store marker data and interpolation table.
C
    JS = N + NM1
    KS = JS + NM2
    LS = KS + NM2 - 1
    D(KS+3) = 0. FOR M =2
    D(LS+4) = 0. FOR M =3

```

```

C.....
DO 50 I = 1, N
    D(I) = X(I)
    D(N+I) = Y(I)
    IF (LOG.EQ.1) D(N+I) = ALOG(Y(I))
    IF (I.LT.2) GO TO 50
    J = JS + I
    D(J) = (D(N+I) - D(NM1+I)) / (D(I) - D(I-1))
    IF (I.LT.3) GO TO 50
    K = KS + I
    D(K) = (D(J) - D(J-1)) / (D(I) - D(I-2))
    IF (I.LT.4) GO TO 50
    L = LS + I
    D(L) = (D(K) - D(K-1)) / (D(I) - D(I-3))
50 CONTINUE

```

```

C.....
    RETURN
C=====
C(B). M POSITIVE:- Interpolate X(I) in the stored array D(I)

```



```

C          The result is returned in Y(I) [which may equal X(I)]
C.....
100 DO 250 J = 1, N
    AX = X(J)
        YY = AX
        IF (AX.EQ.0.0) GO TO 250
C          find interpolation segment INT
    INT = 2
    DO 150 I = 2, NM2
150     IF (AX.GT.D(I)) INT = I
C          calculate Y(J)
    IMT = INT + 2
                                           TOP XVAL

    NS = NM1 *4 + INT
    YY = D(NS)
    NM3 = NM1 - 2
C...
    DO 200 I = 1, 3
        NS = NS - NM3 - I
200     YY = YY* (AX - D(IMT-I) ) + D(NS)
C...
    IF (LOG.EQ.1) YY = EXP(YY)
250 Y(J) = YY
C.....
    RETURN
    END

```