



URSI GASS 2020

Rome, Italy

29 August - 5 September 2020



# A Microwave Imaging System for the Detection of Targets Hidden behind Dielectric Walls

R. Cicchetti<sup>(1)</sup>, V. Cicchetti<sup>(1)</sup>, S. Costanzo<sup>(2)</sup>, P. D'Atanasio<sup>(3)</sup>, A. Fedeli<sup>(4)</sup>,  
M. Pastorino<sup>(4)</sup>, S. Pisa<sup>(1)</sup>, E. Pittella<sup>(5)</sup>, E. Piuzzi<sup>(1)</sup>, C. Ponti<sup>(6)</sup>,  
A. Randazzo<sup>(4)</sup>, M. Santarsiero<sup>(6)</sup>, G. Schettini<sup>(6)</sup>, and O. Testa<sup>(1)</sup>

<sup>(1)</sup>Sapienza University of Rome, Rome, Italy; <sup>(2)</sup>University of Calabria, Rende (CS), Italy; <sup>(3)</sup>Italian National Agency for New Technologies, Energy and Sustainable Economic Development, Casaccia Research Centre, Rome, Italy; <sup>(4)</sup>University of Genoa, Genoa, Italy; <sup>(5)</sup>Pegaso University, Rome, Italy; <sup>(6)</sup>Roma Tre University, Roma, Italy



## Introduction

- ❑ Localization of **targets** in **unreachable regions** (e.g., inside buildings) is important in **many applications** [1][2]:
  - Police and military force missions
  - Fire-fighting and rescue operations
- ❑ Microwave systems are very promising for such task → Although several **methods** and **systems** have been proposed, there is still the need for further advancements.
- ❑ A new prototype of imaging system is presented.
- ❑ It allows two different working modalities, in order to be able to work remotely from the wall or in direct contact with it.
- ❑ Some preliminary validation studies are shown.



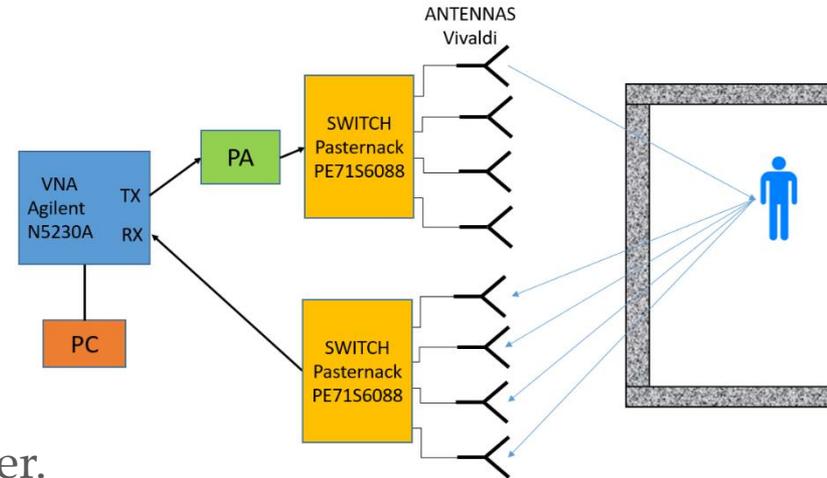
Research activity funded by MIUR under the PRIN2015 project U-VIEW, grant no. 20152HWRSL.

[1] M. G. Amin, Through-the-Wall Radar Imaging. Boca Raton, FL: CRC Press, 2011.

[2] M. Pastorino and A. Randazzo, Microwave Imaging Methods and Applications. Boston, MA: Artech House, 2018.

## Overview of the developed setup

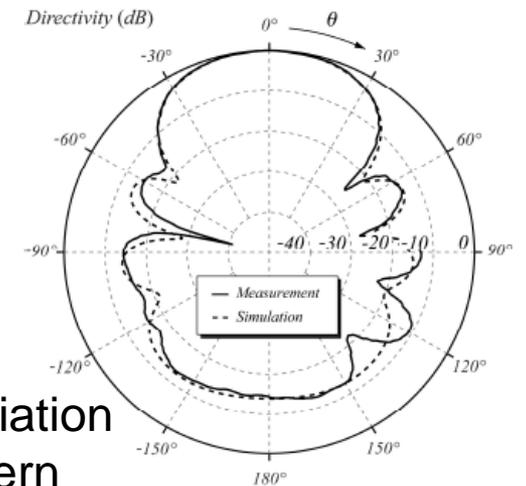
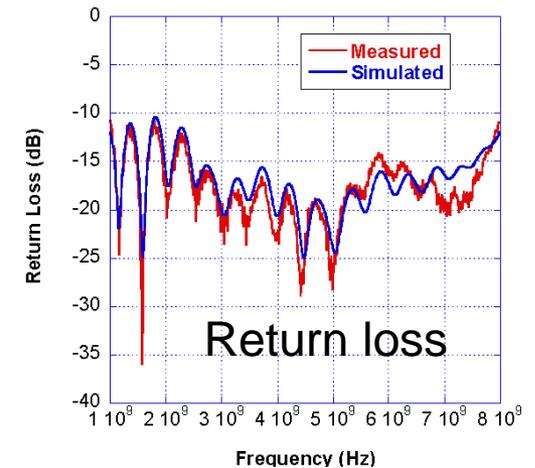
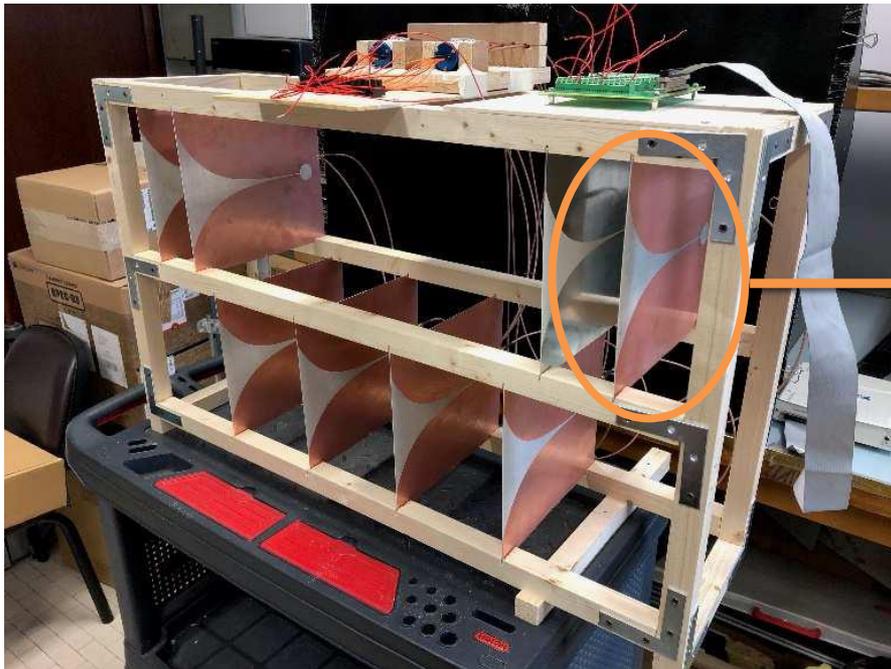
- Two possible operating modalities.
- **Remote modality:**
  - MIMO array of 16 Vivaldi antennas connected to a VNA through a switch.
  - A power amplifier in the transmitting channel is used to increase the TX power.



- **Proximity modality:**
  - Bessel beams are used to focalize in specific regions behind the wall.
  - A circular waveguide equipped with an exciter suitable to generate a Bessel beam @  $\sim 8.7$  GHz has been developed.
  - A printed antenna placed in the neighboring of the launcher is used to receive the field scattered by the target.

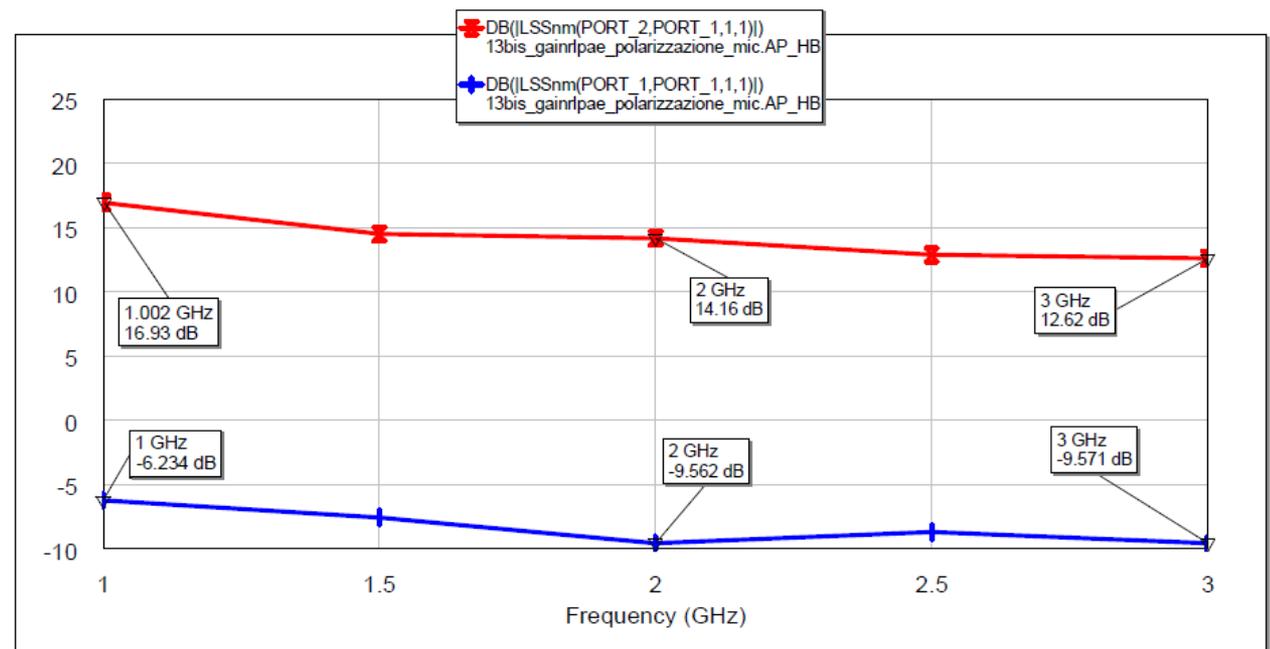
# Overview of the remote system

- The remote system is based on a MIMO structure composed by Vivaldi antennas, which allows to synthesize a monostatic array of 16 elements with spacing 3.75 cm.



## Overview of the remote system

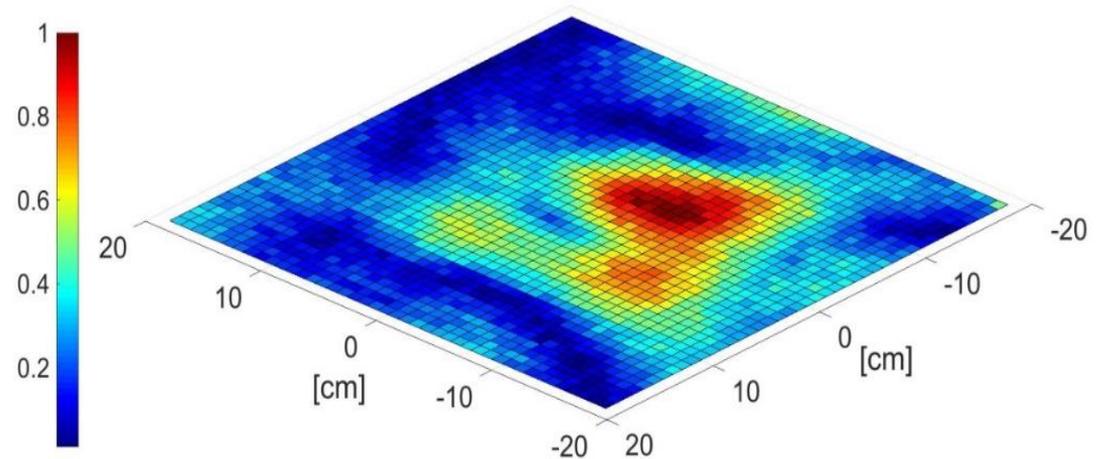
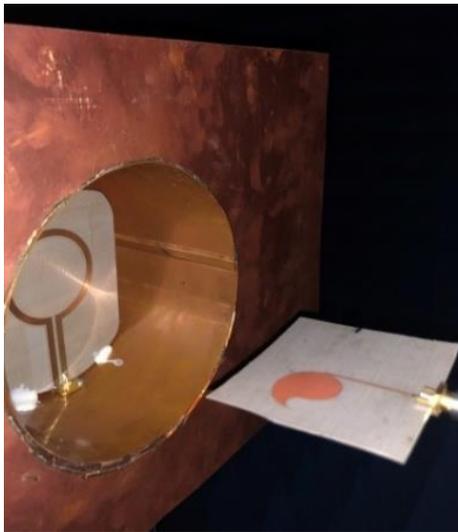
- A class A amplifier based on a GaN transistor (Polyfet GP1441) has been designed to achieve a maximum transmit power of 10 W.



Return loss and gain of the developed amplifier

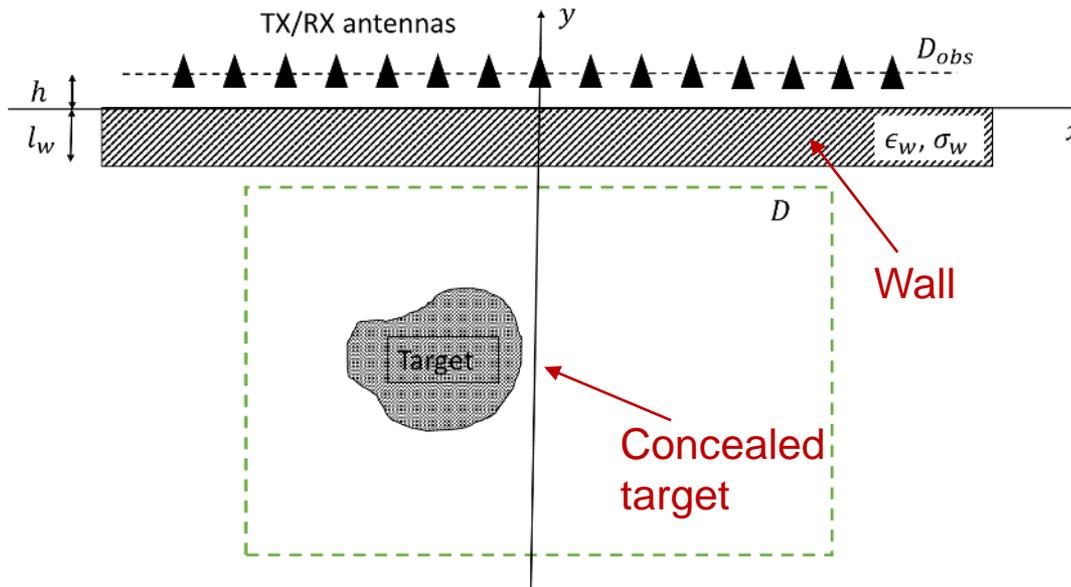
## Overview of the proximity system

- ❑ The proximity system allows to exploit the focusing capabilities of Bessel-beam sources.
- ❑ To this end, a Bessel beam launcher based on a circular waveguide containing three anular rings has been developed.



Distribution of the electric field produced by the developed Bessel launcher.

# Through-wall scattering modeling



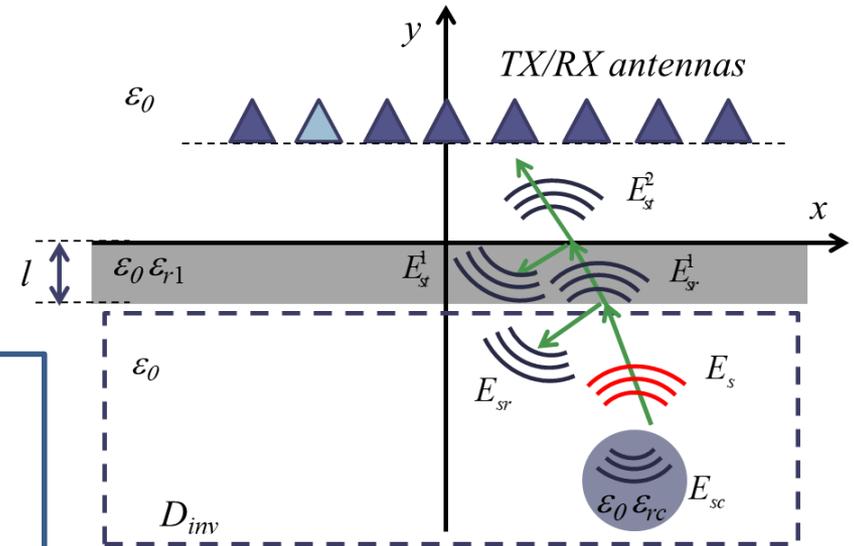
The inverse scattering problem is reduced to a 2D scalar problem ( $\mathbf{r} = (x, y)$  and scalar fields)

- ❑ **Homogeneous wall** with thickness  $l_w$  and dielectric properties  $\epsilon_{r,w}, \sigma_w$
- ❑ **Cylindrical targets**, located inside a known area  $D_{inv}$
- ❑ The scene is illuminated by **TMz incident electric fields**  $e_i(\mathbf{r})$ .
- ❑ Total field  $E_t(\mathbf{r})$  is collected by a receiving antenna in different positions located in the measurement domain  $D_{obs}$



# Through-wall scattering: forward modeling

- A forward model based on the cylindrical wave approach [1] has been developed to model the through-wall scenario.



## Scattered-transmitted field in medium 0

$$E_s(x, y) = V_0 \sum_{q=1}^N \sum_{m=-\infty}^{+\infty} i^m c_{qm} TW_m^{2,0}(x, y; d_q)$$

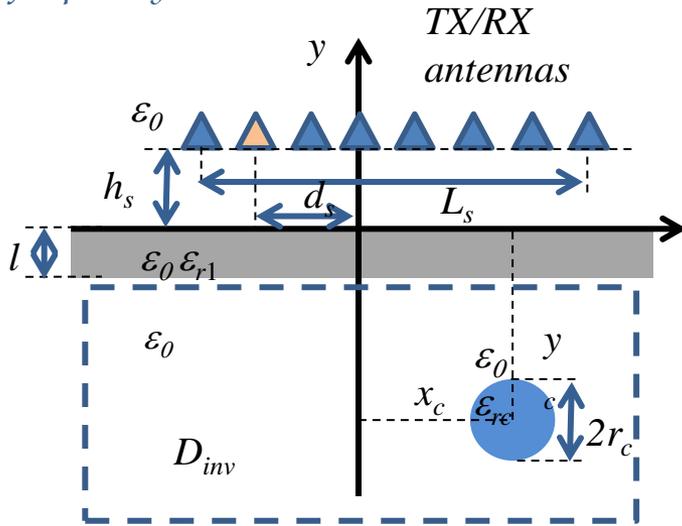
- The basis functions are Reflected Cylindrical waves, expressed through the plane-wave spectrum

$$TW_m^0(x, y; h_q) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} T_{10}(k_{\parallel}) T_{21}(k_{\parallel}) F_m[-k_2(h_q - l), k_{\parallel}] e^{i\sqrt{1-(k_2 k_{\parallel})^2}x} e^{ik_2 k_{\parallel}(y-d_q)} dk_{\parallel}$$

Fresnel reflection coefficient at the interface between medium 1/medium 0 and medium 2/medium 1

# An example of forward modeling

frequency = 1 GHz



## Target

center  $(x_c, y_c) = (-20 \text{ cm}, 60 \text{ cm})$   
 radius  $r_c = 7.5 \text{ cm}$   
 relative permittivity  $\epsilon_{rc} = 3$

## Wall

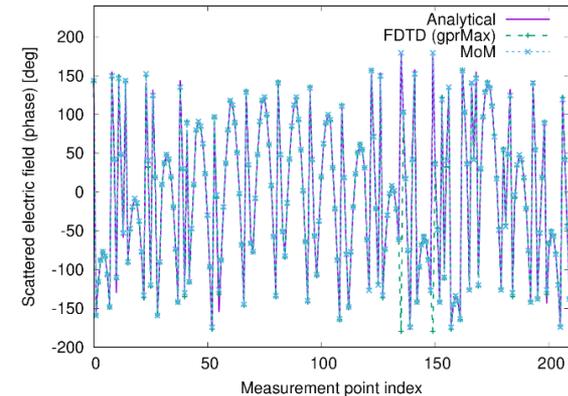
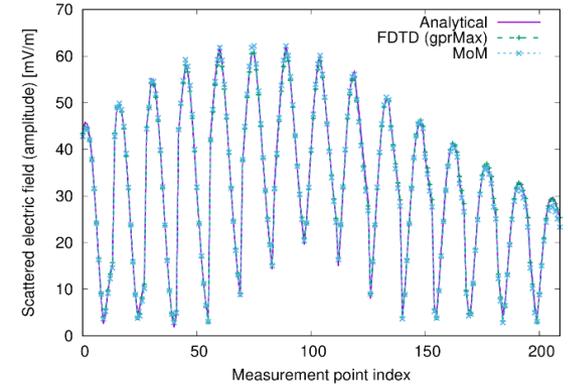
relative permittivity  $\epsilon_{r1} = 4$   
 thickness  $l = 20 \text{ cm}$

## CWA

$M_t = 9$  truncation order  
 $M = 19$  system order

## MoM

$N = 900$  square subdomains  
 side length = 0.005 m





## Through-wall scattering: inverse modeling

- The inverse problem is based on the formulation of the TW problem in terms of a first-order linearized integral equations involving a multi-layer 2D Green's function [1][2], i.e.,

$$E_s(\mathbf{r}_{RX}^{s,m}) \cong \int_D \chi(\mathbf{r}') g_{tw}(\mathbf{r}', \mathbf{r}_{TX}^s) g_{tw}(\mathbf{r}_{RX}^{s,m}, \mathbf{r}') d\mathbf{r}' = G_{tw} \chi(\mathbf{r}_{RX}^{s,m})$$

- where

Generalized reflection and transmission coefficients

$$g_{tw}(\mathbf{r}, \mathbf{r}') = \frac{j}{4\pi} \int_{-\infty}^{+\infty} \frac{e^{j\zeta(x-x')}}{\gamma_1} \begin{cases} e^{-j\gamma_0|y-y'|} + R e^{-j\gamma_0(y+y')}, & y \geq 0 \\ T e^{j\gamma_0(y+l-y')}, & y \leq -l_w \end{cases} d\zeta$$

[1] F. Soldovieri and R. Solimene, "Through-Wall imaging via a linear inverse scattering algorithm," IEEE Geosci. Remote Sens. Lett., Oct. 2007.

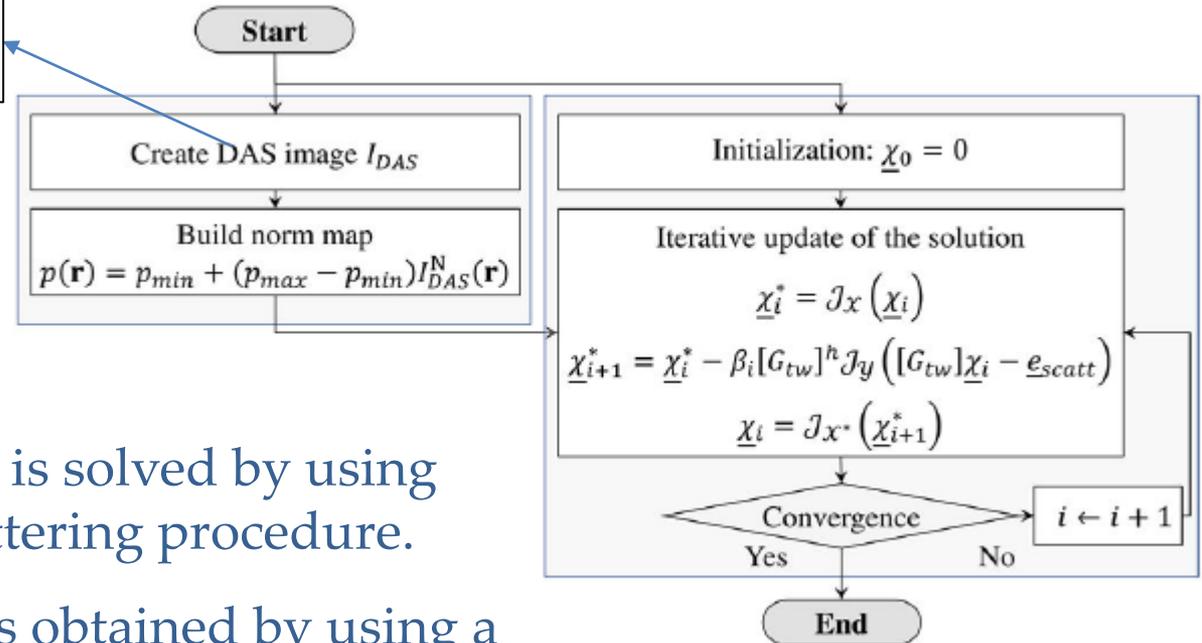
[2] M. Pastorino and A. Randazzo, Microwave Imaging Methods and Applications. Boston, MA: Artech House, 2018.



# Through-wall scattering: inverse modeling

$$I_{DAS}(\mathbf{r}) = \sum_{f=1}^F \sum_{s=1}^S \sum_{m=1}^M E_{scatt}^s(\mathbf{r}_{RX}^{s,m}) e^{j\omega_f(\tau_{TX}^s(\mathbf{r}) + \tau_{RX}^{s,m}(\mathbf{r}))}$$

Delays computed by means of Fermat's principle



- ❑ The inverse problem is solved by using a hybrid inverse-scattering procedure.
- ❑ A first initial image is obtained by using a Delay-And-Sum scheme with wall compensation [1].
- ❑ Such an image is used to define the exponent function for a Landawber iterative scheme in variable-exponent Lebesgue spaces [2].

[1] S. Pisa et al., "Comparison between delay and sum and range migration algorithms for image reconstruction in through-the-wall radar imaging systems," IEEE J. Electromagn. RF Microw. Med. Biol., 2018.

[2] C. Estatico, A. Fedeli, M. Pastorino, and A. Randazzo, "Quantitative microwave imaging method in Lebesgue spaces with nonconstant exponents," IEEE Trans. Antennas Propag., 2018.

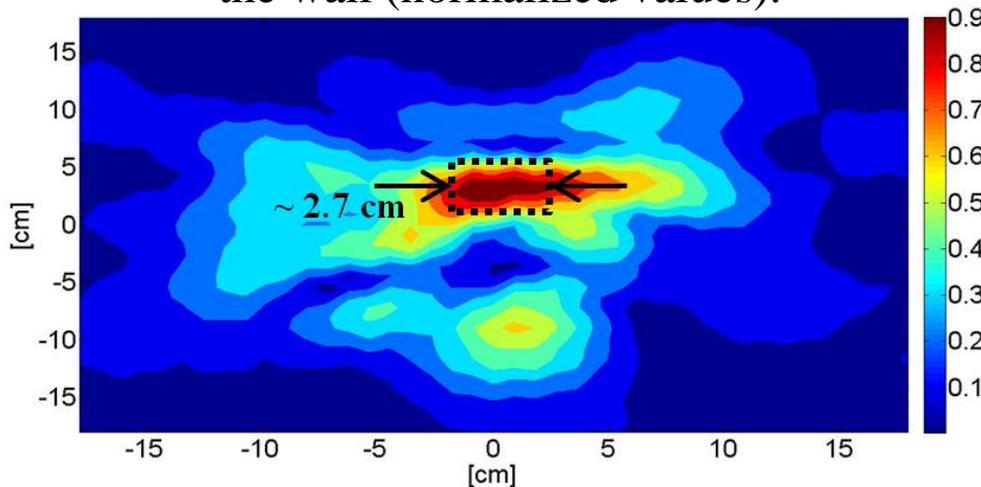
## Experimental results – Proximity modality

- An analysis of the focusing capabilities of Bessel beams in through-the-wall scenarios has been performed.
- A stratified wall composed of a 10 mm plasterboard layer and a 20 mm wood layer has been considered.

### Dielectric properties of the wall layers

	Dielectric Constant	Loss Tangent
Plasterboard	1.40	0.007
Wood	1.76	0.067

Measured field transmitted behind the wall (normalized values).



**A very good focusing of the transmitted field is obtained.**



## Experimental results – Remote modality

### □ Measurement parameters

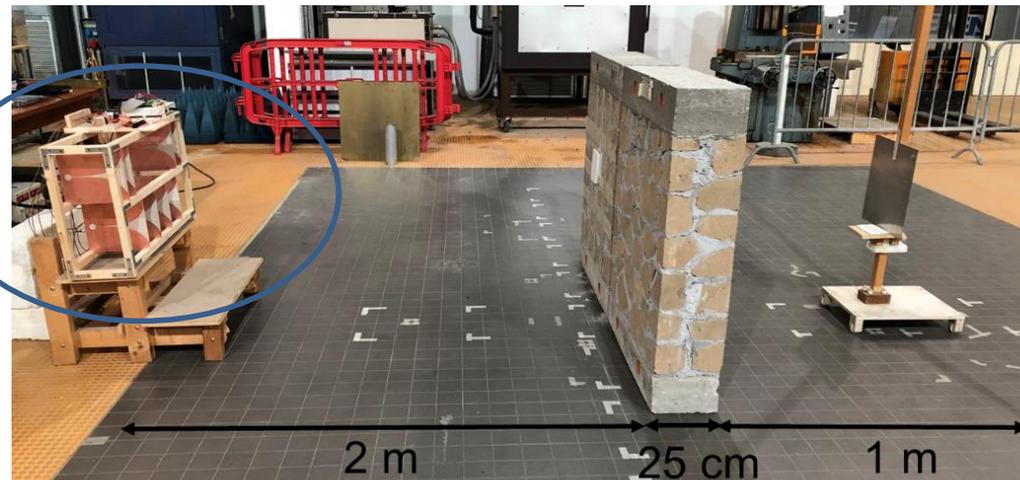
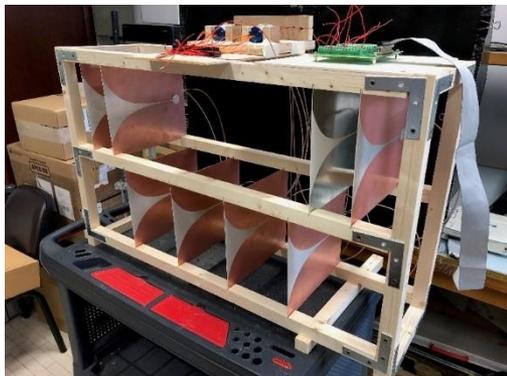
- Brick wall 1.2 m high, 1.8 wide and 0.25 m thick, with estimated relative dielectric permittivity 4.5.
- MIMO array with 16 Vivaldi antennas 2 m away from the wall.
- Frequency-stepped measurements between 1 GHz and 3 GHz with a step of 4 MHz.

### □ Target parameters

- Metallic plate with sides 36×42 cm, located 1 m from the wall and 60 cm from the floor.

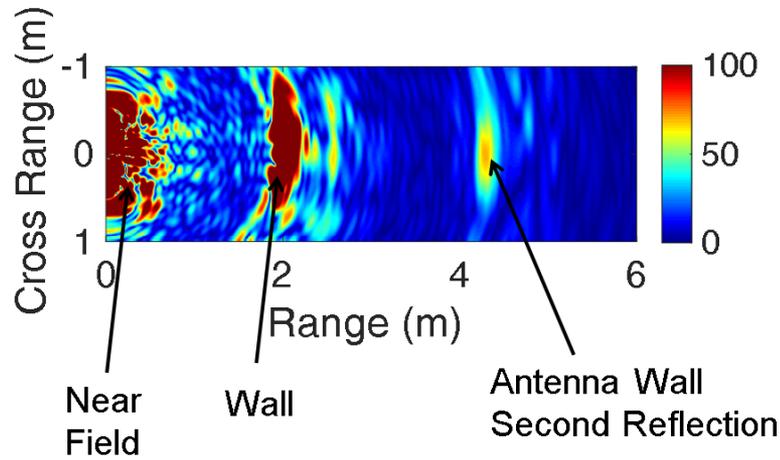
### □ Inversion procedure parameters

- Maximum number of iterations, 100; threshold on the relative variation of the residual, 0.01; range of the norm parameter, [1.4, 2.0].

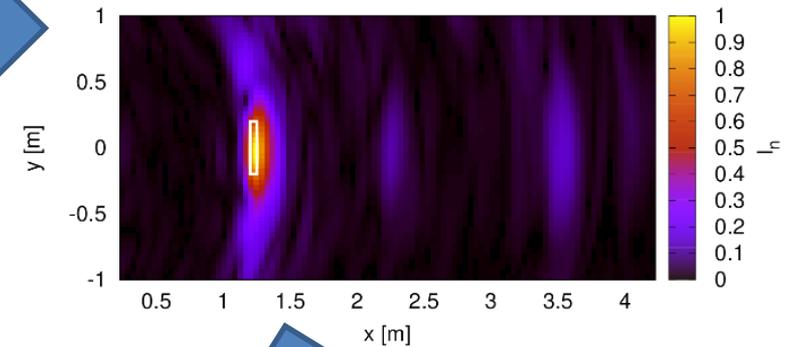


## Experimental results – Remote modality

### Raw DAS reconstructions (unfocused)

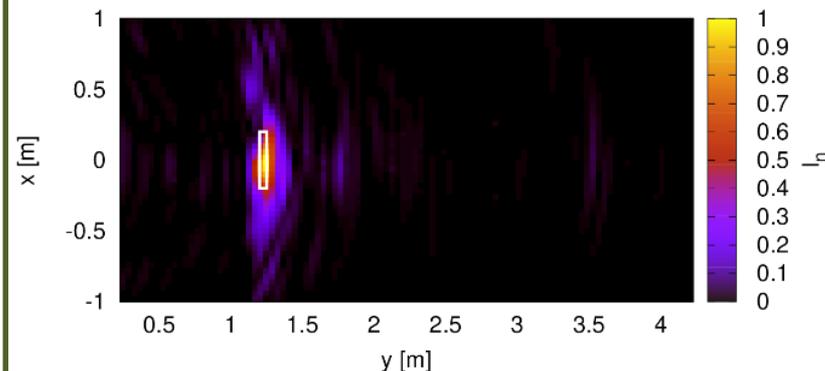


### DAS reconstructions with wall compensation



- The developed hybrid procedure allows to obtain an **accurate reconstruction**, in which the target is **correctly localized and shaped**.
- Moreover, the background is **clean from artefacts**, which are instead present in the DAS image.

### Hybrid approach reconstruction





## Conclusions

- ❑ A new prototype of imaging system for through-the-wall imaging has been presented and experimentally validated.
- ❑ It allows two different working modalities, in order to be able to work remotely from the wall or in direct contact with it.
- ❑ In the remote case, measurements are acquired by using a MIMO array and are processed by an efficient inverse-scattering procedure.
- ❑ In the proximity modality, Bessel beams are exploited in order to obtain highly-focused fields behind the wall.
- ❑ **Further activities** will be devoted to a more comprehensive validation of the system.