Abstract

The large constellations of spacecraft planned for use in cislunar space (on the Lunar surface, in Lunar orbit, and in the vicinity of the Lunar Gateway) require new solutions for positioning, navigation and timing (PNT). Here, I describe COMPASS (Combined Observational Methods for Positional Awareness in the Solar System), a spacecraft navigation system to provide cost-effective techniques for the positioning of large numbers of spacecraft in cislunar space. COMPASS will use beacons that emit coherent ultra-wideband signals designed to be interoperable with existing and future Very Long Baseline Interferometry (VLBI) networks. Using differential VLBI, COMPASS will provide rapid determination of the interferometric phase delay with picosecond level accuracy during routine VLBI observing sessions. Multi-baseline phase-referenced COMPASS-VLBI observations with simultaneous calibrator observations should thus enable sub-meter accuracy transverse positioning and meter level lunar orbit determination using with small femtospacecraft beacons and a few seconds of observation per position determination.

1 Introduction

Some of the earliest VLBI observations of any sort were done using the Apollo Lunar Surface Experiments Package (ALSEP) transmitters, which had very narrow bandwidths of a few kHz at S-band (the network was spread in frequency from 2275.5 to 2279.5 MHz). Initial experiments without any calibrator sources were used to determine relative positions of the ALSEP transmitters on the Moon to within “about 30 m along the earth-moon direction and about 10 m in each of the two transverse coordinates” [1]. Later work developed differential VLBI including quasar calibrator sources [2], but unfortunately this work was terminated when the program was canceled.

Although there was subsequently intensive development of spacecraft navigation using VLBI, including tracking of both Cassini and Huygens at Saturn and Titan (see, e.g., [3, 4, 5, 6]) VLBI was not applied again in lunar operations until 2007, when the Japanese Selene spacecraft carried two small subsatellites into lunar orbit. These small spacecraft, Rstar and Vstar, were used in the VRAD (differential VLBI RADio sources) mission in order to improve the knowledge of the lunar gravity field, particularly on the far side [7]. VRAD, using same-beam differential VLBI (where all radio sources are simultaneously observably by each radio antenna), demonstrated < 1 picosecond differential phase delay errors. The VRAD VLBI data were used operationally to decrease the VRAD orbit errors from 100s of meters to about 10 meters [8] and improve the resulting gravity field.

The Chang’e 3 lunar lander landed on the Moon on 14 December, 2013, as part of Chinese Lunar Exploration Program (CLEP). VLBI was used to track the Chinese Chang’e 3 lander during its landing sequence [9] and after landing; in addition VLBI was used to determine rover-lander relative positions on the lunar surface [10, 11]. The relative positions of the rover were determined at the meter level and the absolute position of the lander to within about 10 meters. Chang’e 3 was also observed in geodetic VLBI experiments under the IVS OCEL (Observing Chang’e-3 with VLBI) Research and Development project [12]. Note that the OCEL observations were inserted into conventional geodetic observing sessions and did not hamper their geodetic use.

2 Extending the Space Service Volume to the Moon

The current Space Service Volume (SSV) extends from 3000 to 36,000 km altitude, [13], denoting the region near and above the GPS and GNSS constellations where it is typically not possible to perform near-instantaneous GNSS point solutions, but instead the GNSS pseudorange observable must be used in a integrated orbital solution. Ashman et al. [14] invested GPS performance above the current SSV. At altitudes > 36,000 km all GPS observation is “over the shoulder” (i.e., observing satellites on the other side of the Earth) and the use of the GPS signal sidebands is essential to routine GPS availability, making up about 80% of the signals received at the highest altitudes. Simulation of navigation system errors on lunar trajectories exhibited considerable Geometrical Dilution of Precision (GDOP), km level
Table 1. The Beamwidth at the Moon from the Earth for possible antenna and frequency choices. All beamwidths are significantly less than the lunar radius of \( \sim 1738 \) km; differential phase VLBI will thus benefit from multiple antennas at each location or geodetic reference beacons at the Moon.

<table>
<thead>
<tr>
<th>Network</th>
<th>Antenna Diameter</th>
<th>Frequency 8.4 GHz</th>
<th>Frequency 13 GHz</th>
<th>Frequency 43 GHz</th>
</tr>
</thead>
<tbody>
<tr>
<td>VLBA</td>
<td>25 m</td>
<td>550 km</td>
<td>360 km</td>
<td>110 km</td>
</tr>
<tr>
<td>NG-VLA</td>
<td>18 m</td>
<td>760 km</td>
<td>500 km</td>
<td>150 km</td>
</tr>
<tr>
<td>VGOS</td>
<td>13 m</td>
<td>1060 km</td>
<td>680 km</td>
<td>-</td>
</tr>
</tbody>
</table>

radial errors, 100 m lateral errors, and high correlations between the radial position and the spacecraft clock offset.

A continuously available lunar beacon service providing one-way autonomous tracking would help to extend the SSV to cislunar space and the lunar surface; especially once a lunar communication relay system is available. There is no intrinsic reason why COMPASS position fixes could not processed in a matter of minutes and relayed immediately, if needed, to the spacecraft operators or to the spacecraft itself.

3 Tracking Lunar Spacecraft with Very Long Baseline Interferometry

The basic equation for relatively narrow band coherent VLBI SNR is [3]

\[
SNR = t_{int} \frac{\eta \pi D^2}{4 k T_{sys}} \left( \frac{P_{transmit}}{4 \pi f R^2} \right)
\]

where \( \eta \) is the net VLBI receive antenna efficiency, \( k \) the Boltzmann constant, \( T_{sys} \) the system temperature, \( D \) the antenna diameter, \( R \) the distance to the source, \( P \) the transmitter power, \( f \) is the UWB loss factor, about 11.3 for 802.15.4a, and \( G_{transmit} \) the beacon gain (assumed to be \( \sim 1 \)). Assuming typical values for the 25 meter VLBA telescopes, with \( T_{sys} = 26.6 \) K and \( \eta = 0.55 \), a milliWatt UWB transmitter at the lunar distance could in theory be detected with an SNR of 10 with 1 second integration. On the other hand, radio observers without knowledge or interest in the UWB signal structure, i.e., those treating it as an incoherent broadband source would, at the lunar distance, observe a broadband signal power of 0.4 milliJanskies, well below the sensitivity of most terrestrial users (and with many natural radio sources with similar or greater power in the sky).

With signal multiplexing enabling multiple beacons to broadcast simultaneously, the existing and planned VLBI networks could potentially track thousands of spacecraft carrying suitable VLBI beacons, providing a new source of financial support for VLBI. Terrestrial VLBI observations can provide differential phase data with picosecond accuracy [8], corresponding (with a 1.5 Earth radius baseline) to an instantaneous transverse accuracy of \( \sim 3 \times 10^{-11} \) radians or \( \sim 7 \) mas. That would produce a transverse positioning error of \( \sim 1 \) cm and a radial (parallax) error of \( \sim 0.5 \) meters, assuming observations from a suitably distributed network of VLBI stations on the Earth. (Note that near the lunar limb, e.g., in the polar regions, “transverse” and “radial” will be significantly mis-aligned with the Lunar topography.)

4 COMPASS

COMPASS was first proposed (under a different name) as part of FAIM, the Femtospacecraft Asteroid Impact Mission [15], a proposal to provide instruments and VLBI beacons for the asteroid moon Didymos-\( \beta \) for its use in a planetary defense experiment. The Moon is much closer than the Didymos impact test, and it is thus correspondingly easier to provide a useful VLBI signal from a small module. The full scale COMPASS module shown in Figure 1 would be (at least during the lunar day) able to provide rapid determination of surface positions or lunar orbiters using multi-baseline phase-referenced COMPASS VLBI observations with simultaneous or near simultaneous calibrator observations. The module in Figure 1 would be able to act autonomously; smaller (credit-card sized) beacons could also provide useful data on a pre-programmed transmission schedule.

Low power (\( \lesssim 10 \) milliW) COMPASS beacon signals could be observed using, for example, the new VGOS VLBI system [16], the Very Long Baseline Array (VLBA) [4] or the proposed NG-VLA [17]. The goal is to provide nanoradian or better accuracy astrometry and meter-level or better transverse position accuracies with a relatively small number of observations per positioning fix. COMPASS would also support single frequency broadcast modes for simpler (and less accurate) navigation solutions. In either case COMPASS node would be assigned a unique identifier (a lunar equivalent of a Ethernet MAC address) which would used to multiplex the signal so that same beam interferometry could be performed with multiple beacons simultaneously in the same VLBI beam.

Table 1 provides information on the possible COMPASS frequencies of operations and the resulting beamwidths at the highest operating frequencies for the terrestrial antennas involved. As the typical beamwidths are smaller than the Moon, same-beam observations will typically not be possible. Both VGOS and the NG-VLA have (or are planned to have) multiple collocated antennas, allowing for the simultaneous observations of COMPASS beacons and VLBI calibrators.

COMPASS beacon carried by surface landers could serve as geodetic control points on the Lunar surface, directly tying the Lunar, planetary and extra-galactic reference frames, especially if the beacon was collocated with a suitable lunar laser ranging retroreflector [18]. These measurements would meet a number of scientific goals; transverse VLBI measurements of lunar rotation would nicely
complement the on-going program of radial measurements from Lunar Laser Ranging (LLR). VLBI beacon observations would also directly tie the lunar reference frame into the International Celestial Reference Frame [19] and would make it possible to extend the LLR reference frame to all surface or orbital operations.

4.1 COMPASS UWB

COMPASS will use Commercial-off-the-Shelf (COTS) technology to the maximum extent possible. Crucial to the COMPASS accuracy goals is the production of coherent multi-frequency Ultra-WideBand (UWB) GHz beacons [20] and we are investigating the use or modification of the IEEE 802.15.4-a-2011 standard for this purpose. This offers sub-nanosecond pulses with a 3.9 MHz (or higher) pulse repetition rate in 500 MHz or 1 GHz bandwidth channels. There is COTS industrial equipment available that supports centimeter level positioning and local communications networks with support for up to 11,000 communications nodes. Evaluation of this technology is on-going.

5 Conclusions

COMPASS will be a positioning system suitable for expanding the SSV into cislunar space based small and relatively inexpensive UWB beacons. COMPASS techniques and technology will be applicable to a wide variety of exploration missions and commercial endeavors, a combined COMPASS beacon and Lunar Laser Ranging (LLR) laser retroreflector on the Lunar surface would provide an immediate and strong scientific return, directly tying the Lunar reference frame into the International Celestial Reference Frame (ICRF) and providing independent estimates of Lunar orbit and librations, providing complementary data useful in tests of General Relativity and in determining the internal dynamics of the Moon. Surface beacons would also provide phase reference sources for orbiting beacons in support of time-critical Lunar operations, such as during landing navigation.

References


