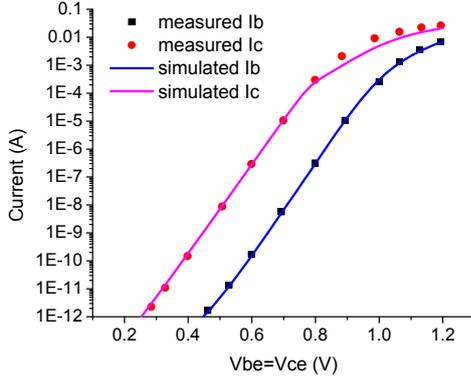




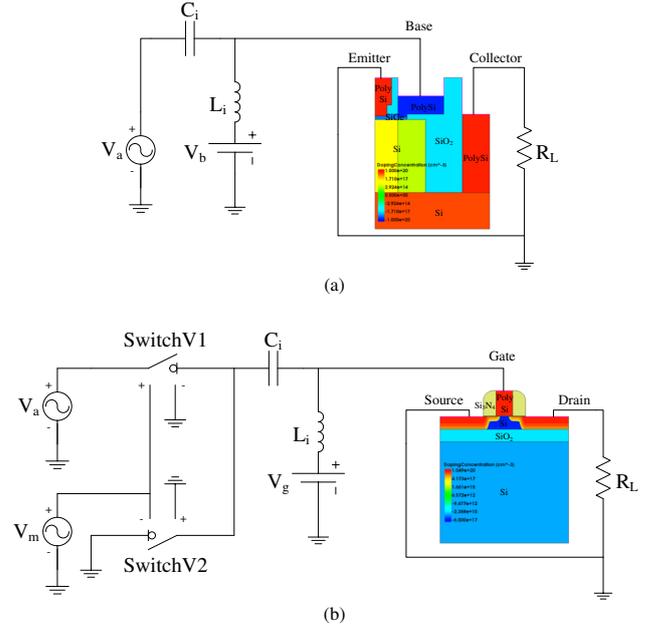
**Table 1.** Summary of the device parameters for the SiGe HBT TCAD model.

| Device parameters   | Value         |
|---|---------------|
| Emitter width $W_e$ ( $\mu\text{m}$ )                             | 0.21          |
| Base width $W_b$ ( $\mu\text{m}$ )                                | 0.02          |
| Collector width $W_c$ ( $\mu\text{m}$ )                           | 0.4           |
| Sub-Collector width $W_{sc}$ ( $\mu\text{m}$ )                    | 0.2           |
| Emitter length $L_e$ ( $\mu\text{m}$ )                            | 0.13          |
| Base length $L_b$ ( $\mu\text{m}$ )                               | 0.35          |
| Collector length $L_c$ ( $\mu\text{m}$ )                          | 0.15          |
| Emitter contact length $L_{ec}$ ( $\mu\text{m}$ )                 | 0.18          |
| Base contact length $L_{bc}$ ( $\mu\text{m}$ )                    | 0.15          |
| Collector contact length $L_{cc}$ ( $\mu\text{m}$ )               | 0.15          |
| SiGe and Base PolySi overlap length $L_{ov}$ ( $\mu\text{m}$ )    | 0.05          |
| Shallow trench isolation (STI) length $L_{ox}$ ( $\mu\text{m}$ )  | 0.2           |
| PolySi doping ( $\text{cm}^{-3}$ )                                | $1\text{e}20$ |
| Base doping ( $\text{cm}^{-3}$ )                                  | $3\text{e}18$ |
| Selectively Implanted Collector (SIC) doping ( $\text{cm}^{-3}$ ) | $1\text{e}16$ |
| Collector doping ( $\text{cm}^{-3}$ )                             | $1\text{e}15$ |
| Sub-collector doping ( $\text{cm}^{-3}$ )                         | $2\text{e}19$ |



**Figure 2.** Comparison of the simulated I-V characteristics with the measured data [19].

sis of the THz response, where the THz signal is not modulated. This configuration could be simulated with either transient or harmonic balance (HB) simulations in Sentaurus. For the transient simulation, the THz voltage response at the collector or the drain could be extracted from the Fourier transform of the collector or drain voltage waveform at the zero frequency or dc component. For the HB simulation, the THz voltage response could be simply extracted from the zero or dc component of the collector or drain voltage when the simulation is completed. The schematic in Fig. 3 (b) is the typical configuration used in practical measurements, where the THz signal  $V_a$  is modulated by another ac voltage source  $V_m$  with a modulation frequency  $f_m$  much lower than the THz signal frequency  $f$ . This configuration could only be simulated with the time-varying transient simulation in Sentaurus. The THz response could also be extracted from the Fourier transform of the collector or drain voltage waveform, but at the mod-

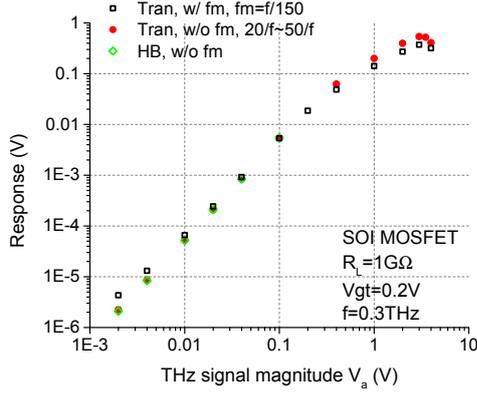


**Figure 3.** Schematics of mixed mode simulation for THz detection with the TCAD models (a) without modulation and (b) with modulation.

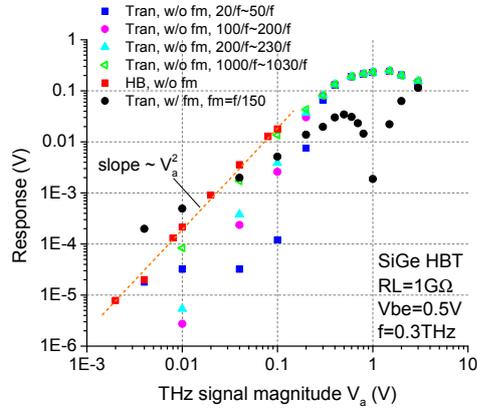
ulation frequency  $f_m$ .

The time-varying schemes with or without modulation have been validated in [22]. To evaluate the HB scheme, we use the SOI MOSFET TeraFET TCAD model in [22]. Fig. 4 shows the comparison of the simulated drain response as a function of the THz signal magnitude for the SOI MOSFET model. The response of the transient simulation without modulation is extracted from the waveform with the time range between  $20/f$  and  $50/f$ . The transient simulation results with and without modulation are in good agreement and the results with modulation deviate from the quadratic response (proportional to  $V_a^2$ ) due to the non-ideal voltage-controlled switches in Fig. 3 (b). This is consistent with the results of the AlGaAs/InGaAs HFET in [22]. Also, the HB simulation results agree with the transient simulation results without modulation, which validates the HB approach for THz response simulation in Sentaurus. At high THz signal magnitude, the HB simulation suffers from convergence problems and transient simulation could be used.

The different schemes are then applied to the SiGe HBT TCAD simulations. Fig. 5 shows the dependence of the simulated response on the THz signal magnitude for the SiGe HBT model. For the transient simulation scheme without modulation, different time ranges for the collector voltage waveform are used for the extraction of the THz response. The comparison shows that the time-varying simulation with modulation may not be proper for the SiGe HBT response simulation, since the HBT may not have large enough input impedance to minimize the influence of the non-ideal voltage-controlled switches. Also, the time range of the collector voltage waveform for the THz response ex-



**Figure 4.** Simulated drain response at 0.3 THz as a function of the THz signal magnitude for the SOI MOSFET TCAD model with different schemes.

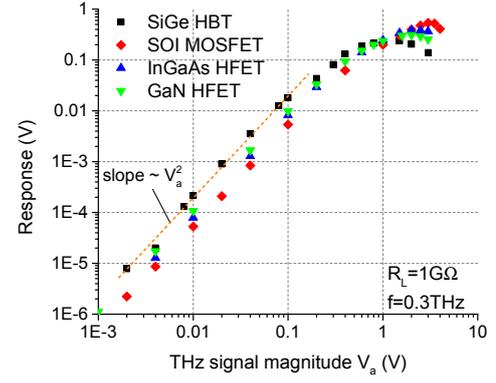


**Figure 5.** Simulated collector response at 0.3 THz as a function of the THz signal magnitude for the SiGe HBT TCAD model with different schemes.

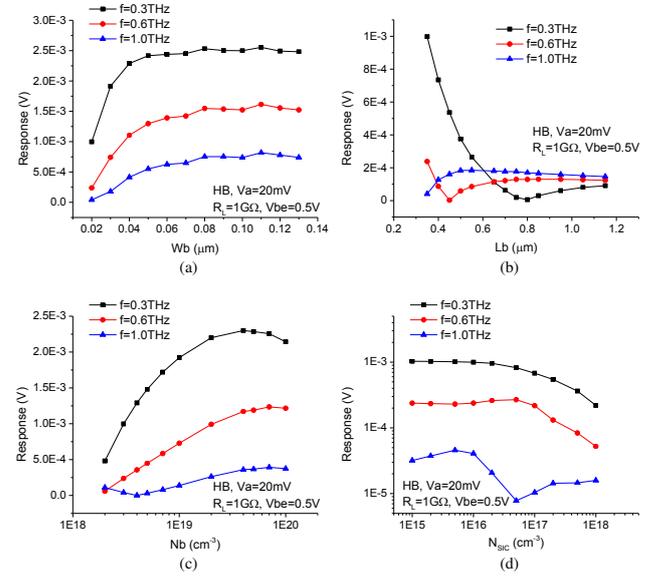
traction from the Fourier transform could have a significant effect on the results at the low or medium  $V_a$  ranges. It could be seen that the longer time the transient simulation takes, the more accurate results are obtained since they are getting closer to the HB simulation results which could be considered as the correct results. At high intensities ( $V_a > 0.2$  V), however, the results are the same for different time ranges used for the response extraction. This suggests an efficient simulation approach for the SiGe HBT response, which is to use HB simulations in the low and intermediate  $V_a$  ranges and transient simulation without modulation in the high  $V_a$  range. The results also show the quadratic response at the low and medium intensity range and the response saturation at the high intensity range for the SiGe HBT, which is consistent with the  $V_a$  dependence of the response for the TeraFET detectors [22].

#### 4 Comparison with THz TeraFET detectors

Using the proposed scheme, we obtain the dynamic range of the THz response for the SiGe HBT model and compare the results with the TeraFET TCAD models in [22]. Fig. 6 shows the comparison of the dynamic ranges. The results



**Figure 6.** Comparison of simulated collector or drain response at 0.3 THz as a function of the THz signal magnitude for the SiGe HBT and TeraFET TCAD models.



**Figure 7.** Simulated collector response to the variations of the device design parameters for the SiGe HBT TCAD model at different frequencies.

are obtained using the transient simulation without modulation, except for the SiGe HBT model in the 1 mV and 0.1 V range of the THz signal magnitude; where the response is obtained from the HB simulation. It could be seen that these devices have comparable dynamic ranges, and SiGe HBTs could work as efficient THz detectors as the TeraFETs implemented in different material systems.

#### 5 Response to design parameter variation

The mixed mode HB simulation could be a very useful tool for the physical design of the THz detector, since it runs much faster than the time-varying transient simulation. By running the HB simulation at the intermediate  $V_a$  range, we explore the SiGe HBT response to the variations of the device design parameters at different frequencies. Fig. 7 shows the simulated results for various base parameter values including the width, length, and doping, as

well as the collector doping values. Therefore, high detector response could be obtained by optimizing the device parameters, such as adopting medium base width, small base length, high base doping and low SiC doping. These results also suggest an effective approach of using THz scanning to test Si BiCMOS VLSI, since the THz response could be different between the working and defective devices or the authentic and counterfeit chips.

## 6 Conclusion

The TCAD model for the SiGe HBT detector is in good agreement with the measured current-voltage characteristics and shows the quadratic response at the low and medium intensity ranges and the response saturation at the high intensity range. The dynamic range is comparable with the dynamic range of the various TeraFET detectors. The mixed mode harmonic balance simulation for the SiGe HBT response to the variations of the device parameters provides an efficient approach for the detector design and optimization. The simulation results could be applied in the non-destructive testing of Si BiCMOS VLSI with THz radiation.

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