

EMI IN WIRELESS COMMUNICATIONS: FULL-SCALE BEHAVIOURAL-LEVEL SIMULATION (INVITED)

Sergey Loyka

*School of Information Technology and Engineering (SITE), University of Ottawa
161 Louis Pasteur, Ottawa, Ontario, Canada, K1N 6N5, Email: sergey.loyka@ieee.org*

ABSTRACT

Main challenges in electromagnetic interference (EMI) modeling and simulation for modern and future wireless communication systems and networks are addressed in this paper. It is emphasized that there exists a big difference between simulating analog and digitally-modulated systems. A computationally-efficient approach for the EMI analysis of wireless systems and networks by behavioural-level numerical simulation is proposed. Rapid growth of PCs' computational power allows to implement full-scale simulation of modern wireless systems and networks at the behavioural level.

INTRODUCTION

Wireless communication systems experience today unprecedented growth. The number of systems increases almost exponentially, in parallel with the increase in number and quality of services offered. According to some predictions, by year 2010 the number of wireless subscribers will exceed the number of wireline subscribers [1]. In view of very limited spectrum available and large concentration of system over limited space (dense urban or indoor environment), the potential for mutual interference is tremendous. The large-scale introduction of broadband wireless systems (i.e., 3G), which is foreseen for near future [2], will make this problem even more important and more difficult to solve due to several reasons: (1) the larger bandwidth of the system results in more interference produced and makes the system more susceptible to external interference, (2) smart antennas, which is a key component in 3G systems [3,4], are more susceptible to interference due to active circuitry in their structure [5], (3) BLAST architecture, which is very likely to be implemented in the near future due to its unprecedented spectral efficiency [6], makes use of multiple transmit (Tx) and receive (Rx) branches and, hence, produces and receives much more interference, (4) more high-quality services offered by such systems at reasonable price will likely increase the number of subscribers and, hence, the number of systems in limited space and spectrum available.

Generally speaking, the performance of wireless communication networks can be severe degraded by mutual interference between various radio systems sharing the same space and the same frequency band and, thus, must be carefully taken into account in the design stage. The techniques proposed and successfully used in the past [7,8] are largely based on empirical or semi-empirical models developed for analog systems and may be not accurate for modern digital systems.

In this paper, we discuss main challenges in EMI modeling and simulation for wireless communication networks, main differences between EMI analyses for analog and digital systems and propose a computationally-efficient approach for system (behavioural) -level simulation of wireless systems at the physical layer (i.e., taking into account almost all the hardware imperfections) which can be efficiently combined with the existing methods of simulation at the signal processing level providing in this way a technique for the simulation of the entire communication link, starting for the source of information and up to the destination point. The computational efficiency of this approach is expected to be high enough to allow the simulation of real-world systems and even networks under real-world conditions in reasonable time and using reasonable computational resources (i.e., PCs rather than supercomputers).

EMI EFFECTS IN ANALOG AND DIGITAL WIRELESS SYSTEMS

The mutual interference between wireless systems is presently taken into account mainly during the frequency planning stage and in an oversimplified way, i.e. no comprehensive Tx and Rx models are employed, only few basic parameters (carrier frequency, bandwidth, Tx power, Rx sensitivity and selectivity etc.) are accounted for. The main reason for this is that there is no accurate and computationally-efficient technique available for more accurate and comprehensive analysis. Thus, even carefully made frequency planning does not guarantee the absence of EMI in any scenario.

In general, all the interference effects may be divided into two large groups: (1) linear effect and (2) nonlinear effect. Modeling and simulation of linear effects in communication systems do not present a serious problem and can be carried out in a conventional way [9]. On the contrary, accurate modeling and simulation of nonlinear effects in modern communication systems is a big challenge [10]. Thus, we concentrate our discussion on modeling and simulation of nonlinear effects.

Some possible kinds of nonlinear interference and distortions for wireless communication systems are the following [7, 8]:

1. Spurious radiation of transmitters: harmonics and sub-harmonics, intermodulation products (IMP), noise etc. Note that the intermodulation radiation can be caused by an external signal (from a nearby transmitter) as well as by several carriers (in CDMA systems, for example) in the transmitter's power amplifier.
2. Spurious responses of receivers: adjacent, image and intermediate frequency (IF) channels.
3. Nonlinear behavior of receivers may also cause the system performance degradation (desensitization, IMPs, local oscillator noise and harmonics' conversion etc.).

Analytical and semi-empirical methods were extensively used in the past for the analysis of these effects [7, 8]. Those methods were quite simple and allowed one to get some insight into the system operation. However, the accuracy of those methods is rather poor. Besides, the analysis of complex systems (present-day digital wireless systems) is rather difficult if not possible at all to do by the old methods.

Digital communication systems present additional challenge for the EMC/EMI analysis because computational resources required for such an analysis is much higher for digital systems than for analog ones [10]. For example, for a RF power amplifier employed in an analog system, IMP levels present its important performance parameter (among others). The traditional two-signal simulation is sufficient to predict this performance parameter. On the contrary, if this amplifier is employed in a digital system, other performance measures are used – adjacent channel power ratio (ACPR), error vector magnitude (EVM) etc., because the traditional analog parameters (i.e., IMPs, IPs etc.) do not represent adequately the digital system performance [10]. In order to predict these new parameters, multi-tone simulation should be used (typically, with few thousand or even tens of thousand tones), which is much more computationally-expensive. A similar set of new parameters should be employed to predict adequately the performance of digital wireless receivers.

The considerations above suggest that the only likely candidate for the EMC/EMI analysis of present-day and future wireless systems is a numerical simulation approach. A system-level analysis, which is required in our case, cannot be done at the circuit-level due to high complexity of the wireless system and of the digitally modulated signals. Besides, the circuit-level simulation would require too much characterization data. Thus, behavioral-level techniques (also known as “black-box” techniques) should be used for such a problem [11-13]. We further discuss one such technique – the instantaneous quadrature modeling technique.

INSTANTANEOUS QUADRATURE TECHNIQUE

The main idea behind the instantaneous quadrature technique to combine the quadrature modeling technique and the discrete technique in order to build a simulation technique which can model the circuit or system behavior over wide frequency and dynamic ranges taking into account both AM-AM and AM-PM conversions [11-13]. In order to model signals and systems over a wide frequency range, the instantaneous values of the signals must be used, not the complex envelope. In order to model the AM-PM conversion, the quadrature modeling structure should be used for the nonlinear element modeling. Thus, the modeling process consists of the following items:

1. Linear filters are modeled in the frequency domain (the same as for the discrete technique).
2. Nonlinear elements are modeled in the time domain using the quadrature structure, but the instantaneous signal values are used, not the complex envelope.
3. The transform from the frequency (time) domain to the time (frequency) domain is made by IFFT (FFT) (very computationally efficient).
4. The Hilbert transform [11] is used to calculate in-phase and quadrature components,

$$x_Q(t) = \hat{x}(t) = \int_{-\infty}^{\infty} \frac{x(\tau)}{t - \tau} d\tau, \quad x_I(t) = x(t), \quad (1)$$

where $x_I(t)$ and $x_Q(t)$ – are instantaneous in-phase and quadrature components of the signal, $\hat{x}(t)$ is the Hilbert-conjugate signal of $x(t)$. In fact, we use the Hilbert Transform in the frequency domain to calculate the quadrature components because it does not require numerical integration and, thus, is much more computationally efficient: $x_Q(t) = IFFT(-j \cdot S(\omega))$ for $\omega \geq 0$, where $S(\omega) = FFT(x(t))$ is the signal's spectrum. The signal itself is the in-phase component, and the Hilbert's conjugate signal is the quadrature component.

A system of two integral equations is used in order to convert the envelope transfer function into the instantaneous ones:

$$\frac{4}{\pi} \int_0^1 k_I(A_{in}t) \frac{t^2 dt}{\sqrt{1-t^2}} = K(A_{in}) \cos \Phi(A_{in}), \quad \frac{4}{\pi} \int_0^1 k_Q(A_{in}t) \sqrt{1-t^2} dt = K(A_{in}) \sin \Phi(A_{in}) \quad (2)$$

where k_I and k_Q – are the instantaneous in-phase and quadrature transfer factors. Note also that using (2) only the even parts of the transfer factors can be calculated. In order to find the odd parts, some additional characteristics should be used (for instance, the second harmonic transfer factor). As a rule, the amplitude transfer characteristics can be measured or simulated using a circuit-level simulator, thus we need to solve equations (2) for k_I and k_Q . This can be done using the method of moments. If we use piecewise constant basis functions and a point matching technique, the matrices of these equations appear to be upper triangular ones, so the systems of linear equations can be solved analytically (this semi-analytical approach speeds up computations substantially).

Fig. 1 gives an illustration of the nonlinear element modelling. It should be noted that the transfer function of the quadrature channel is not a usual transfer function in a conventional sense: it depends not only the input of the quadrature nonlinearity (x_Q) but also on the input of the entire structure (x_{in}) i.e., in fact, on the input of the in-phase nonlinearity (x_I) [11]. Consequently, we cannot use the usual methods of the transformation of the envelope transfer function into the instantaneous one. At the same time, the transfer function of the in-phase channel is a usual transfer function and those methods can be applied in this case.

If one needs to simulate even-order nonlinear products, then odd parts of the instantaneous transfer factors must be determined. It can be done using the second-order envelope characteristics (second harmonic zone AM-AM and AM-PM functions or second-order IMP at the output for the two-tone input):

$$\frac{4}{\pi} \int_0^1 k_I(A_{in}t) \frac{t(2t^2-1)}{\sqrt{1-t^2}} dt = K_2(A_{in}) \cos(\Phi_2(A_{in})), \quad \frac{8}{\pi} \int_0^1 k_Q(A_{in}t) t \sqrt{1-t^2} dt = K_2(A_{in}) \sin(\Phi_2(A_{in})) \quad (3)$$

where $K_2(A_{in})$ is the second-order envelope transfer factor and $\Phi_2(A_{in})$ is the second-order AM-PM characteristic. We can solve the integral equations (3) using the traditional method of moments approach. But, as practical experience shows, it requires even more sample points than for the even parts. Thus, it is much efficient to use the semi-analytical approach proposed above.

APPLYING INSTANTANEOUS QUADRATURE TECHNIQUE TO WIRELESS SYSTEMS

Let us now consider the simulation of typical wireless subsystems/systems using the instantaneous quadrature technique. Fig. 2 illustrates the simulation of a single stage RF amplifier (either power or low noise). The input and output filters model the matching networks, and the quasy-memoryless nonlinear elements model the amplifier nonlinearity (both AM-AM and AM-PM). Using this approach, we may simulate other RF and IF stages (like mixers

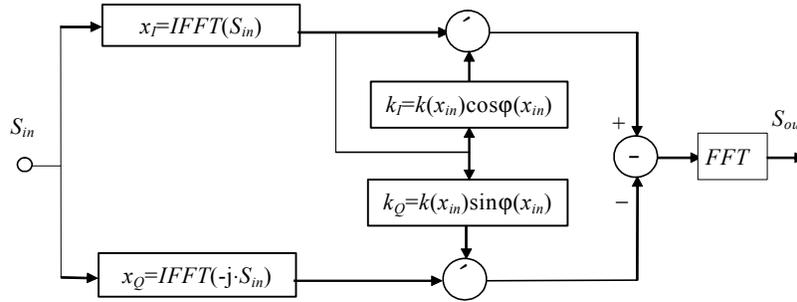


Figure 1. Modeling broadband nonlinear element by the instantaneous quadrature technique.

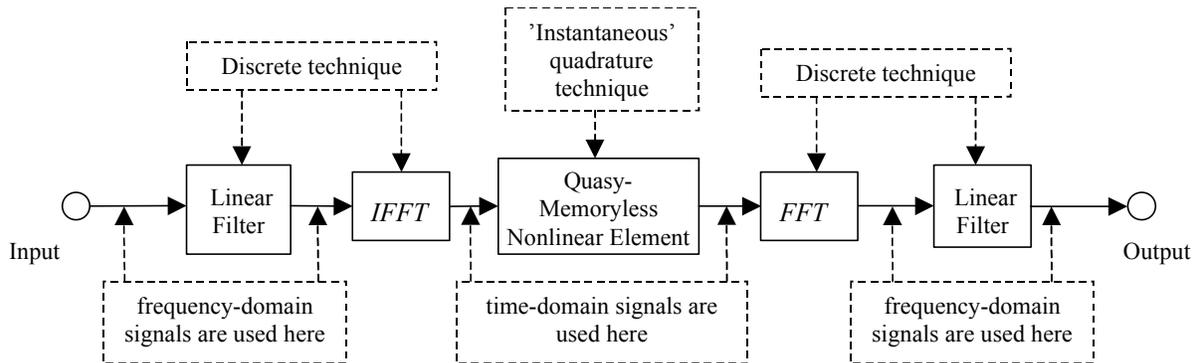


Figure 2. Simulating a single-stage radio amplifier by the instantaneous quadrature technique.

and IF amplifiers) and even detectors [13] in a computationally-efficient way. Further, using the black-box approach, we may simulate the entire link and network operation under real-world conditions and signals.

The simulation of a wireless transmitter using the instantaneous quadrature technique is quite straight-forward: we do it in the same way as for the quadrature modeling technique. The power amplifier is considered to be the main source of interference and distortions in this case (however, other stages can also be simulated). Figure 3 shows the simplified block diagram of a wireless receiver (digital signal processing is after detector), in a form suitable for the EMC/EMI analysis (filters are included in the corresponding blocks). Automatic gain control, automatic frequency control and synchronization loops are not shown because they are not easy to simulate using the techniques above in its present form. This is an important topic for future research. The simulation of a wireless receiver is not so simple because many its components can contribute to the overall interference and distortions. Thus, we consider (i.e. simulate) the receiver block diagram step by step: low-noise amplifier, local oscillator plus mixer, IF filter and IF amplifier, detector and baseband signal processing part. It should be noted that (i) frequency response is taken into account in every stage, and (ii) detector simulation is possible using the technique proposed that enables us to go further to the simulation of baseband signal processing. DSP can be simulated using either the traditional approach [9] or the instantaneous quadrature technique. Thus, the instantaneous quadrature technique can be used for the EMC/EMI simulation of the entire wireless communication link over wide frequency and dynamic ranges.

The technique has been demonstrated to be able to predict accurately the nonlinear performance of RF amplifiers (i.e., IMPs, harmonics, desensitization etc.) over wide frequency and dynamic ranges in a computationally-efficient way, so the simulation of digital systems is also possible. It should be noted that the instantaneous quadrature technique can be easily combined with the linear simulation techniques [9], which predict the performance of baseband signal processing. However, much work remains to be done before practical and efficient simulation (software) tool will be available.

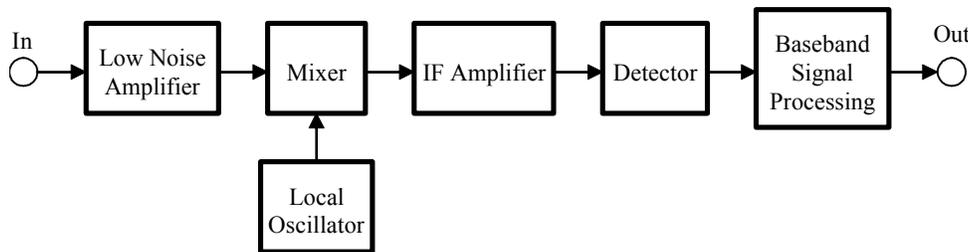


Figure 3. Simplified block diagram of a wireless receiver; digital signal processing is done after the detector.

References

- [1] M. Shafi et al, Wireless Communications in the Twenty-First Century: A Perspective, Proceedings of IEEE, vol. 85, N. 10, Oct. 1997, pp. 1622-1638.
- [2] K.Biesecker, The Promise of Broadband Wireless, IT Professional, vol. 2, N. 6, Nov.-Dec. 2000, pp.31-39.
- [3] J.H. Winters, Smart Antennas for Wireless Systems, IEEE Personal Communications, Feb. 1998, pp. 23-27.
- [4] K. Sheikh et al, Smart Antennas for Broadband Wireless Access Networks, IEEE Communications Magazine, vol. 37, N. 11, Nov. 1999, pp. 100-105.
- [5] S.L. Loyka, "The Influence of Electromagnetic Environment on Operation of Active Array Antennas: Analysis and Simulation Techniques," *IEEE AP Magazine*, Dec. 1999, vol. 41, N 6, pp. 23 –39.
- [6] G.D. Golden et al, 'Detection Algorithm and Initial Laboratory Results Using V-BLAST Space-Time Communication Architecture', *Electronics Letters*, vol. 35, No. 1, pp.14-16, 7th January 1999. (on-line: <http://www.bell-labs.com/project/blast/>).
- [7] J. Gavan, "Principles of Radio System and Relevant EMI Environmental Effects, Analysis and Computation," in R. Perez (ed.), *Handbook on Electromagnetic Compatibility*, New York, Academic Press, 1995.
- [8] D.D. Weiner, "Nonlinear Interference Effects in EMC", *Supplement to the Proc. of 10th Int. Zurich Symp. on EMC*, Zurich, March 1993, pp.114-127.
- [9] M.C. Jeruchim, P. Balaban, K.S. Shanmugan, *Simulation of Communication Systems*, Plenum Press: New York, 1992.
- [10] J. F. Sevic, M. B. Steer and A. M. Pavio, "Nonlinear analysis methods for the simulation of digital wireless communication systems," *International Journal of Microwave and Millimeter-Wave Computer-Aided Engineering*, vol. 6, No. 3, 1996, pp.197-216.
- [11] S. Loyka, J.R. Mosig, "New behavioral-level simulation techniques for RF/microwave applications. Part I: Basic concepts", *Int. Journal of RF and Microwave Computer-Aided Engineering*, vol. 10, no. 4, July 2000, pp. 221-237.
- [12] S. Loyka, J.R. Mosig, "New behavioral-level simulation techniques for RF/microwave applications. Part II: Approximation of nonlinear transfer functions", *Int. Journal of RF and Microwave Computer-Aided Engineering*, vol. 10, no. 4, July 2000, pp. 238-252.
- [13] S.L. Loyka, J.R. Mosig, New Behavioral-Level Simulation Technique for RF/Microwave Applications. Part III: Advanced Concepts, *International Journal of RF and Microwave Computer-Aided Engineering*, v. 12, N.2, pp.206-216, Mar. 2002.